Scilab Textbook Companion for Introduction to Nuclear Engineering by J. R. Lamarsh and A. J. Baratta¹

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Book Description

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Scilab numbering policy used in this document and the relation to the above book.

Exa Example (Solved example)

Eqn Equation (Particular equation of the above book)

AP Appendix to Example(Scilab Code that is an Appednix to a particular Example of the above book)

For example, Exa 3.51 means solved example 3.51 of this book. Sec 2.3 means a scilab code whose theory is explained in Section 2.3 of the book.

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Chapter 2

Atomic and Nuclear Physics

Scilab code Exa 2.1 Number of deuterium atoms

```
1 // Example 2.1
2 clear all;
3 \, \text{clc};
4 // Given data
5 atom_h = 6.6*10^{24};
                                                // Number
      of atoms in Hydrogen
  // Using the data given in Table II.2, Appendix II
6
      for isotropic abundance of deuterium
                                                11
7 \text{ isoab}_{H2} = 0.015;
      Isotropic abundance of deuterium
8 // Calculation
9 totatom_d=(isoab_H2*atom_h)/100;
10 // Result
11 printf('\n Number of deuterium atoms = \%2.1E \n',
      totatom_d);
```

Scilab code Exa 2.2 Atomic and Molecular weight

```
1 // Example 2.2
2 clear all;
3 clc;
4 // Given data
5 // Using the data given in the example 2.2
6 \text{ atwt_016} = 15.99492;
                                                  // Atomic
      weight of O-16 isotope
7
  isoab_016 = 99.759;
                                                 //
      Abundance of O-16 isotope
                                                 // Atomic
8 \text{ atwt}_017 = 16.99913;
      weight of O-17 isotope
9
  isoab_017 = 0.037;
                                                 11
      Abundance of O-17 isotope
10 \text{ atwt_018} = 17.99916;
                                                 // Atomic
      weight of O-18 isotope
11 isoab_018 = 0.204;
                                                 //
      Abundance of O-18 isotope
12 // Calculation
13 atwt_0=(isoab_016*atwt_016 + isoab_017*atwt_017 +
      isoab_018*atwt_018)/100;
14 // Result
15 printf('\n Atomic Weight of Oxygen = \%5.5 \text{ f} \n',
      atwt_0);
```

Scilab code Exa 2.3 Mass and Energy

```
8 rest_mass = me*c^2;
9 // Result
10 printf('\n Rest mass energy of electron = %5.4E ergs
   \n',rest_mass);
11 disp('Expressing the result in joules')
12 // 1 Joule = 10^(-7) ergs
13 rest_mass_j = rest_mass*10^(-7);
14 printf('\n Rest mass energy of electron = %5.4E
   joules\n',rest_mass_j);
15 disp('Expressing the result in MeV')
16 // 1 MeV = 1.6022*10^(-13)joules
17 rest_mass_mev = rest_mass_j/(1.6022*10^(-13));
18 printf('\n Rest mass energy of electron = %5.4f MeV\
   n',rest_mass_mev);
```

Scilab code Exa 2.4 Mass and Energy

```
1 // Example 2.4
2 clear all;
3 \text{ clc};
4
5 // From the result of Example 2.3
6 // \text{Rest mass energy of electron} = 0.5110 \text{ MeV}
7 rest_mass_mev = 0.5110;
                                                           11
8 \text{ me} = 9.1095 * 10^{(-28)};
      Mass of electron in grams
9 // From standard data table
10 // 1 amu = 1.6606 * 10^{(-24)}g
11 amu = 1.6606*10^{(-24)};
12 // Calculation
13 en_eq = (amu/me)*rest_mass_mev;
14 // Result
15 printf('\n Energy equivalent of one amu = \%3.1 \text{ f MeV}
      n',en_eq);
```

Scilab code Exa 2.5 Excited states and radiation

```
1 // Example 2.5
2 clear all;
3 \text{ clc};
4
5 // From the standard data table
                                                    11
6 h = 6.626 * 10^{(-34)};
      Planck's constant in J-s
7 c = 3*10^8;
                                                    // Speed
       of light in vacuum in m/sec
8 // Given data
9 disp('The ionization energy of K shell electron in
      Lead atom is 88keV');
10 E = 88 * 10^3;
                                                    11
      Ionization energy in keV
11 // Expressing the result in joules by using 1 eV =
      1.6022*10^{(-19)} J
12 E = E*1.6022*10^{(-19)};
13 printf("From Planck\''s law of photoelectric effect
      \ln \text{Energy} = (h*c)/\text{lambda}n");
14 // Calculation
15 lambda = (h*c)/E;
16 // Result
17 printf('\n Wavelength of radiation = \%4.3 \text{ Em} \text{ m}',
      lambda);
```

Scilab code Exa 2.6 Activity of radioactive foil

```
1 // Example 2.6
2 clear all;
3 clc;
```

```
4
 5 // Given data
 6 T12 = 64.8;
                                                      // Half
       life = 64.8 hour
 7 \text{ lambda} = 0.693/T12;
                                             // Decay
      constant in hour (-1)
 8 t = 12;
                                                           11
      Analysis time of gold sample in hours
 9 \text{ alpha} = 0.9;
                                                     //
      Activity of gold sample after analysis time
10
11 // 1.
12 // Calculation
13 R = alpha/(1-exp(-lambda*t));
14 // Result
15 printf('\n Theoretical maximum activity = \%3.1 f
      curie (Ci) \langle n', R \rangle;
16
17 // 2.
18 // Calculation
19 // The expression to calculate 80 percent of maximum
       activity is \ln 0.8R = R*(1 - \exp(-lambda*t))
20 t = -\log(0.2) / \text{lambda};
21 // Result
22 printf('\n Time to reach 80 percent of maximum
      activity = \%d hours (n',t);
```

Scilab code Exa 2.7 Nuclear Reaction

```
1 // Example 2.7
2 clear all;
```

```
3 \, \text{clc};
4
5 disp('The reactants are Nitrogen and neutron')
6 // The total atomic number of reactants
7 Z_reactant = 7+0;
8 // The total atomic mass number of reactants
9 A_reactant = 14+1;
10 disp('One of the known product is Hydrogen')
11 Z_H = 1;
                                         // The atomic
     number of Hydrogen
12 \quad A_H = 1;
                                         // The atomic
     mass number of Hydrogen
13 // The atomic number of unknown element
14 Z_unknown = Z_reactant-Z_H;
15 // The atomic mass number of unknown element
16 A_unknown = A_reactant-A_H;
17 // Result
18 printf(" \  For unknown element the atomic number is
      %d and atomic mass number is %d n, Z_unknown,
     A_unknown);
19 // From periodic table
20 disp('The element corresponds to Carbon-14');
```

Scilab code Exa 2.8 Q value of nuclear reaction

```
1 // Example 2.8
2 clear all;
3 clc;
4 
5 disp('The reaction is Tritium(d,n)Helium-4');
6 // Using standard data table of mass in amu
7 M_H3 = 3.016049; //
Atomic mass of Tritium
8 M_He4 = 4.002604; //
Atomic mass of Helium
```

```
9 M_d = 2.014102;
                                                    Atomic mass of Deuterium
                                                    11
10 M_n = 1.008665;
      Atomic mass of neutron
11 // Calculation of total mass of reactants
12 tot_reac = M_H3+M_d;
13 // Calculation of total mass of products
14 tot_prod = M_He4+M_n;
15 // Calculation
16 Q = tot_reac-tot_prod;
17 // Expressing in MeV by using 1 amu = 931.5 MeV
18 \quad Q_{mev} = Q * 931.5;
19 // Result
20 printf(" \ N \ Q value for the reaction = \%5.3 f \ MeV",
      Q_mev);
21 if Q_mev > 0 then
       printf("\n The reaction is exothermic. (n");
22
23 else
       printf("\n The reaction is endothermic. (n");
24
25 \text{ end}
```

Scilab code Exa 2.9 Binding energy

```
Scilab code Exa 2.10 Mass equation
```

```
1 // Example 2.10
2 clear all;
3 \text{ clc};
4
5 // Using standard data table of mass and the
      coefficients of mass equation for Silver -107
6 N = 60;
                                                         //
      Number of neutrons
7 Z = 47;
                                                         //
      Atomic number
8 \quad A = 107;
                                                         //
      Atomic mass number
9 // The coefficients used in mass equation are
10 \text{ alpha} = 15.56;
11 bet = 17.23;
12 \text{ gam} = 0.697;
13 zeta = 23.285;
14 \text{ mn} = 939.573;
                                                         //
      Mass of neutron in terms of energy
15 \text{ mH} = 938.791;
                                                         //
      Mass of proton in terms of energy
16 // Calculation
```

```
17 disp('Using mass equation');
18 M = (N*mn)+(Z*mH)-(alpha*A)+(bet*(A^(2/3)))+(gam*Z
^2/A^(1/3))+(zeta*(A-2*Z)^2/A);
19 // Expressing in amu by using 1 amu = 931.5 MeV
20 M_amu = M/931.5;
21 printf(" Mass = %5.5 f MeV = %5.5 f u \n",M,M_amu);
22 disp('Actual mass = 106.905092 u');
23 // Calculation
24 BE = (alpha*A)-(bet*(A^(2/3)))-(gam*Z^2/A^(1/3))-((
zeta*(A-(2*Z))^2)/A);
25 // Result
26 printf("\n Binding Energy = %4.2 f MeV or %3.1 f MeV/
nucleon \n",BE,BE/107);
27 // The value is different from the answer given in
```

```
the textbook. The textbook answer is wrong.
```

Scilab code Exa 2.11 Energy of Maxwellian distribution

```
1 // Example 2.11
2 clear all;
3 \text{ clc};
4
5 // Given data
                                           // Given
6 T_C = 38;
      temeperature in celsius
7 //The temperature in Kelvin
8 T_K = T_C + 273.15;
9 T_0 = 293.61;
                                           // The
      temperature in kelvin equivalent to 0 deg celsius
                                           // The term 'kT'
10 \ kT = 0.0253;
       in eV at temperature T0
11 // Calculation
12 Ep = 0.5 * kT * (T_K/T_0);
13 Ebar = 3 * Ep;
14 // Result
```

- 15 printf(" Most probable energy of air molecules = %5 .5 f eV \n", Ep);
- 16 printf(" Average energy of air molecules = %5.5 f eV \setminus n",Ebar);

Scilab code Exa 2.12 Atom density

```
1 // Example 2.12
2 clear all;
3 \text{ clc};
4
5 // Given data
6 \text{ rho} = 0.97;
                                                        //
      Density of Sodium in gram/cm<sup>3</sup>
7 // From standard data table
8 \text{ NA} = 0.6022 * 10^24;
                                                        //
      Avagodro number
9 M = 22.99;
                                                        //
      Atomic weight of Sodium
10 // Calculation
11 N = rho*NA/M;
12 // Result
13 printf("Atom density of sodium = \%5.5E atoms/cm<sup>3</sup> \n
      ",N);
```

Scilab code Exa 2.13 Atom density

```
1 // Example 2.13
2 clear all;
3 clc;
4
5 // Given data
```

```
// Density of
6 \text{ rho}_NaCl = 2.17;
      Sodium Chloride (NaCl) in gram/cm<sup>3</sup>
7 // From standard data table
                                              // Avogodro
8 \text{ NA} = 0.6022 \times 10^{24};
      number
9 M_Na = 22.99;
                                              // Atomic weight
       of Sodium (Na)
10 M_C1 = 35.453;
                                              // Atomic weight
       of Chlorine (Cl)
                                              // Molecular
11 M_NaCl = M_Na+M_Cl;
      weight of Sodium Chloride (NaCl)
12 // Calculation
13 N = rho_NaCl*NA/M_NaCl;
14 // As in NaCl, there is one atom of Na and Cl
15 N_Na = N;
16 \ N_Cl = N;
17 // Result
18 printf(" Atom density of Sodium and Chlorine = \%5.4E
       molecules / \text{cm}^3 \setminus \text{n}^*, N);
```

Scilab code Exa 2.14 Atom density

```
1 // Example 2.14
2 clear all;
3 clc;
4
5 // Given data
                                                          11
6 \text{ rho} = 1;
      Density of water in gram/cm<sup>3</sup>
7
8 // 1.
9 M_H = 1.00797;
                                                          //
      Atomic weight of Hydrogen(H)
10 M_0 = 15.9994;
                                                          //
      Atomic weight of Oxygen(O)
```

11 // As in water, there is two atoms of Hydrogen(H)and one atom of Oxygen(O) $12 M = (2*M_H) + M_O;$ // Molecular weight of water 13 // From standard data table 14 NA = 0.6022×10^{24} ; // Avagodro number 15 // Calculation 16 N = rho * NA/M; 17 // Result 18 printf("Atom density of water = %5.5E molecules/cm³ $\langle n, N \rangle$; 1920 / / 2.21 // As in water, there is two atoms of Hydrogen(H) and one atom of Oxygen(O) $22 N_H = 2*N;$ // Atom density of Hydrogen // $23 N_0 = N;$ Atom density of Oxygen 24 // Result 25 printf("Atom density of Hydrogen(H) = %5.4E atoms/cm ^3 \n",N_H); 26 printf("Atom density of Oxygen(O) = %5.4E atoms/cm³ $\langle n, N_0 \rangle;$ 2728 / / 3.29 // Using the data given in Table II.2, Appendix II for isotropic abundance of deuterium $30 \text{ isoab}_{H2} = 0.015;$ 31 // Calculation $32 \text{ N}_{H2} = \text{isoab}_{H2*N}_{H/100};$ 33 // Result 34 printf("Atom density of Deuterium(H-2)= %5.4E atoms/ $cm^3 \ n", N_H2);$

Scilab code Exa 2.15 Atom density

```
1 // Example 2.15
2 clear all;
3 clc;
4
5 // Given data
6 \text{ rho} = 19.1;
                                                           //
       Density of Uranium-235 in gram/cm<sup>3</sup>
7 \text{ wt} = 1500;
                                                           //
       Weight of uranium rods in a reactor in kg
8 \text{ nr} = 0.2;
                                                           //
       Enrichment(w/o) of Uranium - 235
9
10 // 1.
11 // As Enrichment is 20(w/o)
12 \text{ wt}_{U235} = \text{nr}*\text{wt};
                                                           //
      Amount of \text{Uranium} - 235
13 // Result
14 printf("Amount of Uranium -235 in the reactor = %d kg
        \n", wt_U235);
15
16 / / 2.
17 // From standard data table
18 \text{ NA} = 0.6022 * 10^{24};
                                                           11
       Avagodro number
19 M_U235 = 235.0439;
                                                           //
       Atomic weight of \text{Uranium} - 235
20 M_U238 = 238.0508;
                                                           //
       Atomic weight of Uranium-238
21 // Calculation
22 \text{ N}_{U235} = \text{nr*rho*NA/M}_{U235};
                                                           // Atom
       density of \text{Uranium} - 235
23 \text{ N}_{U238} = (1-nr)*rho*NA/M_U238;
                                                           // Atom
```

Scilab code Exa 2.16 Atom density

```
1 // Example 2.16
2 clear all;
3 \text{ clc};
4
5 // Given data
6 \text{ rho}_{02} = 10.5;
                                                           //
       Density of UO2 pellets in gram/cm<sup>3</sup>
7 \text{ nr} = 0.3;
                                                           //
       Enrichment (w/o) of Uranium -235
  // From standard data table
8
9 M_U235 = 235.0439;
                                                           //
       Atomic weight of Uranium-235
10 M_U238 = 238.0508;
                                                           //
       Atomic weight of Uranium-238
11 M_0 = 15.999;
                                                           //
       Atomic weight of Oxygen
12 NA = 0.6022 \times 10^{24};
                                                           11
       Avogodro number
13
14 M = 1/((nr/M_U235)+((1-nr)/M_U238));
15 \text{ M}_{U02} = \text{M} + (2 * \text{M}_{O});
                                                           //
       Molecular weight of UO2
16 \text{ nr}_U = M/M_UO2*100;
                                                           // The
       percent(w/o) of Uranium in UO2 pellet
17 \text{ rho}_U = \text{nr}_U * \text{rho}_U 02/100
                                                           //
       Density of Uranium in g/cm<sup>3</sup>
```

Chapter 3

Interaction of Radiation with Matter

Scilab code Exa 3.1 Neutron collsion

```
1 // Example 3.1
2 clear all;
3 clc;
 4
 5 // Given data
 6 // 1 \text{ barn} = 10^{(-24)} \text{ cm}^2
 7 sigma = 2.6*10^{(-24)};
                                                      // Cross
       section of \operatorname{carbon} -12 in \operatorname{cm}^2
 8 I = 5*10^8;
                                                      // Intensity
        of neutron beam in neutrons/cm<sup>2</sup>-sec
 9 A = 0.1;
                                                      // Cross
       sectional area of the beam in cm^2;
                                                      // Thickness
10 X = 0.05;
        of the target in cm
11
12 // 1.
13 // Using the data given in Table I.3, Appendix II
       for \operatorname{carbon} -12
14 N = 0.08 \times 10^{(24)};
                                                      // Atom
```

```
density in atoms/cm^3
15 // Calculation
16 IR = sigma*I*N*A*X;
17 // Result
18 printf('\n Total interaction rate = %2.1E
            interactions/sec \n',IR);
19
20 // 2.
21 no = I*A; // Neutron
            rate in neutrons/sec
22 // Calculation
23 p = IR/no;
24 printf('\n Probability of collision = %3.2E \n',p);
```

Scilab code Exa 3.2 Probability of nuclear reaction

```
1 // Example 3.2
2 clear all;
3 clc;
4
5 // Given data
                           // Fission cross section of
6 \text{ sigmaf} = 582;
     U-235 on bombardment of neutron in barn
7 sigmay = 99;
                            // Radiative capture cross
     section of U-235 on bombardment of neutron in
     barn
8 // Calculation
9 pf = sigmaf/(sigmaf+sigmay);
10 // Result
11 printf('\n Probability of fission = \%.3 f = \%3.1 f
      percent\n',pf,pf*100);
```

Scilab code Exa 3.3 Neutron collsion

```
1 // Example 3.3
2 clear all;
3 \text{ clc};
4
5 // Given data
6 // Using the data given in the example 3.1
7 N = 0.08 * 10^{(24)};
                                                 // Atom density
       of Carbon -12 in atoms/cm<sup>3</sup>
8 / / 1 \text{ barn} = 10^{(-24)} \text{ cm}^2
9 sigma = 2.6*10^{(-24)};
                                                 // Cross section
        of \operatorname{carbon} -12 in \operatorname{cm}^2
10 I = 5*10^8;
                                                 // Intensity of
       neutron beam in neutrons/cm<sup>2</sup>-sec
11
12 // 1.
13 // Calculation
14 SIGMAt = N*sigma;
15 // Result
16 printf('\n Macroscopic cross section of carbon -12 =
      \%3.2 \text{ f } \text{cm}^{(-1)} \text{ n', SIGMAt};
17
18 / / 2.
19 // Calculation
20 F= I*SIGMAt;
21 // Result
22 printf('\n Collision density in the carbon -12 target
        = \%3.2E collisions/cm<sup>(3)</sup>-sec\n',F);
```

Scilab code Exa 3.4 Mean free path

```
1 // Example 3.4
2 clear all;
3 clc;
4
5 // Given data
```

```
6 E = 100;
                                             // Neutron
      energy in keV
7 // Using the data given in Table II.3, for E = 100
      keV
8 atom_density = 0.0254*10^{(24)};
                                            // Atom density
      of sodium in atoms/cm^3
  // 1 barn = 10<sup>(-24)</sup> cm<sup>2</sup>
9
10 sigma = 3.4*10^{(-24)};
                                             // Microscopic
      cross section of sodium in cm^2
11 // Calculation
12 SIGMA = atom_density*sigma;
13 lambda = 1/SIGMA;
14 // Result
15 printf('\n Macroscopic cross section = \%5.4 f cm<sup>(-1)</sup>
      \langle n', SIGMA \rangle;
16 printf('\n Mean Free Path = \%3.2 f cm\n', lambda);
```

Scilab code Exa 3.5 Absorption cross section

```
1 // Example 3.5
2 clear all;
3 \, \text{clc};
4
5 // Given data
6 \text{ atom\_density\_U235} = 3.48*10^{(-4)}*10^{(24)};
                                                         // Atom
       density of Uranium -235 in atoms/cm<sup>3</sup>
  atom_density_U238 = 0.0483*10^(24);
                                                         // Atom
7
       density of Uranium -238 in atoms/cm<sup>3</sup>
  // 1 barn = 10<sup>(-24)</sup> cm<sup>2</sup>
8
9 sigmaa_U235 = 680.8*10^(-24);
       Absorption cross section of Uranium-235 incm<sup>2</sup>
10 \text{ sigmaa}_{U238} = 2.7*10^{(-24)};
                                                         11
       Absorption cross section of Uranium-238 incm<sup>2</sup>
11 // Calculation
12 SIGMAA=(atom_density_U235*sigmaa_U235)+(
```

```
atom_density_U238*sigmaa_U238);
13 // Result
14 printf('\n Macroscopic absorption cross section = %4
        .3f cm^(-1)\n',SIGMAA);
```

Scilab code Exa 3.6 Scattering cross section

```
1 // Example 3.6
2 clear all;
3 clc;
4
5 // Given data
6 \text{ sigmas}_H_1 = 3;
                                      // Scattering cross
      section of Hydrogen in barn at 1 MeV
7 \text{ sigmas}_0_1 = 8;
                                      // Scattering cross
      section of Oxygen in barn at 1 MeV
8 \text{ sigmas}_H_th = 21;
                                      // Scattering cross
      section of Hydrogen in barn at 0.0253 eV
9 \text{ sigmas_0_th} = 4;
                                      // Scattering cross
      section of Oxygen in barn at 0.0253 eV
10 // Calculation
11 sigmas_H20_1 = (2*sigmas_H_1)+(1*sigmas_0_1);
12 // Result
13 printf('\n Scattering cross section of Water at 1
      MeV = \%d b \setminus n', sigmas_H20_1);
14 // The equation used to calculate the scattering
      cross section at 1 MeV cannot be used at thermal
      energy.
15 printf(' Experimental value of scattering cross
      section of Water at 0.0253 \text{ eV} = \% \text{d b} \ln',103;
```

Scilab code Exa 3.7 Reactor power

```
1 // Example 3.7
2 clear all;
3 \text{ clc};
4
5 // Given data
6 phi = 1*10^{(13)};
                                                          //
      Neutron flux in neutrons/cm<sup>3</sup>
7 v = 64000;
                                                          //
      Volume of research reactor in cm<sup>3</sup>
8 \text{ sigmaf} = 0.1;
                                                          11
       Macroscopic fission cross section in cm^{(-1)}
   // The energy released per fission reaction is 200
9
      MeV
10 // 1 \text{ MeV} = 1.6 * 10^{(-13)} \text{ joule}
11 E = 200 \times 1.6 \times 10^{(-13)};
12 // Calculation
13 fiss_rate = sigmaf*phi;
                                                          //
       Fission rate in neutrons/cm<sup>2</sup>-sec
14 power_cc = E*fiss_rate/10^6;
                                                          //
       Reactor power/cc
15 power = power_cc*v;
16 printf('\n Reactor power of a research reactor = \%d
      MW \langle n', power \rangle;
```

Scilab code Exa 3.8 Elastic scattering

```
1 // Example 3.8
2 clear all;
3 clc;
4
5 // 1 barn = 10^(-24) cm^2
6 // From the Figure 3.4 given in the textbook
7 sigmae = 4.8*10^(-24); //
Experimental cross section of carbon from 0.02eV
to 0.01MeV
```

```
8 // Assuming spherical shape and elstic scattering
9 R = sqrt(sigmae/(4*%pi));
10 // Result
11 printf('\n Radius of carbon nucleus = %3.1E cm\n',R)
;
```

Scilab code Exa 3.9 Radiative capture reaction

```
1 // Example 3.9
2 clear all;
3 clc;
4
5 // Given data
6 \quad E0 = 0.0253;
                                                      11
      Thermal energy in eV
7 / / 1 \text{ barn} = 10^{(-24)} \text{ cm}^2
8 \text{ sigmay}_E0 = 0.332*10^{(-24)};
      Radiative capture cross section at 0.0253 eV in
      \mathrm{cm}^2
9 E = 1;
                                                      11
      Energy in eV at which radiative cross section is
      to be found
10 // Calculation
11 sigmay_E = sigmay_E0*sqrt(E0/E);
12 // Result
13 // Expressing the result in barn
14 printf('\n Radiative capture cross section of
      hydrogen at 1 eV = \%5.4 \text{ f b/n'}, sigmay_E*10^(24));
```

Scilab code Exa 3.10 Energy loss in scattering reactions

1 // Example 3.10
2 clear all;

```
3 \, \text{clc};
4
5 // Given data
                                               // Energy of
6 E = 1;
       neutron in MeV
7 A = 2;
                                                // Atomic
      mass number of deuterium
8 v = 45;
                                               Scattering angle in degree
9
10 // 1.
11 // Calculation
12 E_dash = E/(A+1)^2 *((cosd (v)+sqrt(A^2-(sind(v))^2))
      )^2);
13 // Result
14 printf('\n Energy of scattered neutron = \%4.3 f MeV \
      n',E_dash);
15
16 / / 2.
17 // Calculation
18 E_A = E - E_dash;
19 // Result
20 printf('\n Energy of recoil nucleus = \%4.3 f MeV \n',
      E_A);
21
22 // 3.
23 // Calculation
24 deltau = log(E/E_dash);
25 // Result
26 printf('\n Change in lethargy of neutron on
      collision = \%4.3 \text{ f} \setminus n', deltau);
```

Scilab code Exa 3.11 Neutron absorption rate

1 // Example 3.11

```
2 clear all;
3 clc;
4
5 // Given data
                                                          11
6 phi = 5*10^{(12)};
      Neutron flux in neutrons/cm<sup>2</sup>-sec
  T = 600;
                                                           11
7
      Temperature of neutron in degree
  // Using the data given in Table II.3, Appendix II
8
      for indium
9 N = 0.0383 * 10^{(24)};
                                                          //
      Atom density in atoms/cm<sup>3</sup>
10 / / 1 \text{ barn} = 10^{(-24)} \text{ cm}^2
11 sigmaa_E0 = 194*10^{(-24)};
                                                           11
      Microscopic absorption cross section in cm^2
12 SIGMA_E0 = N*sigmaa_E0;
      Macroscopic absorption cross section in cm^{(-1)}
13 // From Table 3.2
14 \text{ ga}_{600} = 1.15;
                                                           //
      Non 1/v factor at 600 degree celsius
15 // Calculation
16 F_a = ga_600 * SIGMA_E0 * phi;
17 // Result
18 printf('\n Absorption rate of neutrons per cc in
      indium foil = \%4.2E neutrons/cm<sup>3</sup>-sec \n', F_a);
```

Scilab code Exa 3.12 Activity estimation

```
1 // Example 3.12
2 clear all;
3 clc;
4
5 // Given data
6 N = 120;
    fuel rods
```

// Number of

Scilab code Exa 3.13 Fission neutron estimation

```
1 // Example 3.13
2 clear all;
3 \, \text{clc};
4
5 // Using the data given in Table 3.4 and Table II.2
      for uranium
6 v_{235} = 2.418;
                               // Average number of
     neutrons released per fission
                               // Isotropic abundance of
7 y_235 = 0.72;
      Uranium - 235 on the earth
8 sigmaf_235 = 582.2; // Fission cross section
      of Uranium – 235
9 sigmaa_235 = 680.8;
                               // Absorption cross
      section of \text{Uranium}-235
10 N_{235} = y_{235};
                               // Isotropic abundance of
11 y_{238} = 99.26;
      Uranium-238 on the earth
12 \text{ sigmaa}_{238} = 2.7;
                               // Absorption cross
      section of \text{Uranium}-238
```

Scilab code Exa 3.14 Energy released in fission reaction

```
1 // Example 3.14
2 clear all;
3 \, \text{clc};
4
5 // Fission of 1 g of Uranium-235 releases
      approximately 1 MW/day of energy.
6 / / 1 MW/day = 8.64*10^{(10)} J
7 energy_uranium = 8.64*10^{10};
8
9 // 1. Coal
10 h_coal = 3*10^7; // Heat contenet of coal in J/
      kg
11 // Calculation
12 amt_coal = energy_uranium/h_coal;
13 // Result
14 printf('\n Amount of coal required for energy
      equivalent of fission = \%3.2E kg \n or \%3.2f
      metric tons or \%3.2 \,\mathrm{f} short tons\n', amt_coal,
      amt_coal/10<sup>3</sup>, amt_coal*1.10231/10<sup>3</sup>);
15 // The result is expressed in all units of
      commercial importance.
16
17 // 2. Oil
18 h_oil = 4.3*10^7; // Heat contenet of oil in J/
      kg
19 // Calculation
20 amt_oil = energy_uranium/h_oil;
```

```
21 // Result
22 printf('\n Amount of oil required for energy
    equivalent of fission = %3.2E kg \n or %3.2f tons
    or %3.1f barrels\n',amt_oil,amt_oil/10^3,amt_oil
    *6.3/10^3);
23 // The result is expressed in all units of
    commercial importance.
```

Scilab code Exa 3.15 Gamma ray attenuation in materials

```
1 // Example 3.15
2 clear all;
3 \text{ clc};
4
5 // Given data
6 \text{ rho} = 10;
                                                // Density
      of UO2 in g/cm^3
7 \text{ mol}_wt_UO2 = 238+(16*2);
                                                // Molecular
       weight of UO2
                                                // Percent
  per_U = (238/mol_wt_UO2)*100;
8
      by weight of Uranium
9 \text{ per_0} = 100 \text{ - per_U};
                                                // Percent
      by weight of Oxygen
10
11 // Calculation
12 //Using the data given in Table II.4 for uranium and
       oxygen
13 \text{ mup}_U = 0.0757;
                                                // Ratio of
      mass attenuation coefficient to density of
      uranium in cm^2/g
14 \text{ mup_0} = 0.0636;
                                                // Ratio of
      mass attenuation coefficient to density of oxygen
       in cm^2/g
15 mup = (per_U/100*mup_U)+(per_0/100*mup_0);
                                                       // The
       total ratio of mass attenuation coefficient in
```
```
cm^2/g
16 mu = mup*rho;
17 // Calculation
18 lambda = 1/mu;
19 // Result
20 printf('\n Mass attenuation coefficient of Uranium
        dioxide (UO2) = %5.3 f cm^(-1) \n',mu);
21 printf('\n Mean free path = %3.2 f cm \n',lambda);
22 // The answer is marked wrongly in the textbook. But
        the solution is correctly evaluated.
```

Scilab code Exa 3.16 Energy deposition of radioactive samples

1 // Example 3.16 2 clear all; 3 clc;4 5 // Given data 6 E = 0.8;// Average gamma ray energy in MeV $7 I = 3*10^{(11)};$ // Intensity of gamma rays incident on the container in gamma rays/cm $^2 - \sec$ 8 // Using the data given in Table II.5 for iron at 0.8 MeV // Ratio of mass $9 \text{ mup_iron} = 0.0274;$ attenuation coefficient to density of iron in cm 2/g10 // Calculation 11 dep_rate = E*I*mup_iron; 12 // Expressing the result in SI units $13 // 1 \text{ MeV} = 1.6 * 10^{(-13)} \text{ J}$ 14 / / 1 kg = 1000 g15 dep_rate_SI = dep_rate*(1.6*10^(-13)*1000); 16 printf('\n Rate of energy deposited = %3.2E MeV/gScilab code Exa 3.17 Range of charged particles

Chapter 4

Nuclear Reactors and Nuclear Power

Scilab code Exa 4.1 Conversion and Breeding of nuclear fuels

```
1 // Example 4.1
2 clear all;
3 \, \text{clc};
4
5 // Given data
6 // Number of neutrons absorbed by Uranium -238 in
      resonances for every neutron absorbed in Uranium
      -235
7 \text{ n_resonance} = 0.254;
8 // Number of neutrons absorbed by Uranium -238 at
      thermal energy for every neutron absorbed in
      Uranium - 235
9 n_{th} = 0.64;
10 m = 1;
                              // Amount of \text{Uranium} - 235
     consumed in kg
                              // Atomic mass number of
11 A_U = 235;
      Uranium – 235
12 A_Pu = 239;
                              // Atomic mass number of
      Plutonium –239
```

Scilab code Exa 4.2 Production and doubling time of nuclear fuels

```
1 // Example 4.2
2 clear all;
3 \text{ clc};
4
5 // Given data
6 \text{ wPO} = 1;
                             // Total fuel consumption
     rate in terms of kg/day
                            // Amount of Plutonium -239
  M = 500;
7
      in kg at startup of the reactor
  breeding_gain = 0.15; // Breeding gain of the
8
      reactor
9
10 // 1.
11 printf(" The Fast breeder reactor produces %.2f kg
      of plutonium -239 more for every kilogram consumed
      n", breeding_gain);
12 // Calculation
13 // 1 year = 365 days
```

```
14 production_rate = ceil(breeding_gain*365);
15 // Result
16 printf("\n Production rate of plutonium -239 = %3.2f
kg/day = %d kg/year",breeding_gain,
production_rate);
17
18 // 2.
19 // Calculation
20 t_Dl = M/production_rate;
21 t_De = log(2)*t_Dl;
22 // Result
23 printf(" \n Linear doubling time of plutonium fuel
in the reactor = %2.1f years \n",t_Dl);
24 printf(" \n Exponential doubling time of plutonium
fuel in the reactor = %2.1f years \n",t_De);
```

Scilab code Exa 4.3 Nuclear fuel performance

```
1 // Example 4.3
2 clear all;
3 \text{ clc};
4
5 // Given data
                            // Reactor power in MW
6 \text{ power} = 3300;
7 \text{ time} = 750;
                             // Reactor operation time in
      days
                             // Amount of Uranium dioxide (
8 \text{ amt}_{U02} = 98;
      UO2) in metric tons
9 \text{ atwt_U} = 238;
                             // As the enrichment of
      Uranium -235 is 3 w/o the majority portion is
      Uranium – 238
10 \text{ molwt}_0 = 16;
                              // Molecular weight of Oxygen
11
12
13 // 1.
```

```
14 amt_U = amt_UO2*atwt_U/(atwt_U+2*molwt_O);
                                                 11
     Amount of uranium in tonne
15 total_burnup = power*time;
                                                 // Total
      burnup in MWd
16 // Calculation
17 specific_burnup = total_burnup/amt_U;
18 // Result
19 printf(" \n Specific burnup = \%3.2 f MWd/tonne \n",
     specific_burnup);
20
21 / / 2.
22 // Due to fission of 1.05 g of Uranium -235, 1 MWd of
      energy is released.
23 m = 1.05;
24 P = 10^{6};
25 maxth_burnup = P/m;
                                                 //
      Theoritical maximum burnup
26 // Calculation of Fractional burnup
27 bet = specific_burnup/maxth_burnup;
28 // Result
29 printf(" \n Fractional burnup = \%3.2 f percent \n",
     bet *100);
30 // Due to approximation of specific burnup value,
     there is a slight change in fractional burnup
     value as compared to the textbook value.
```

Scilab code Exa 4.4 Plant availability factor and capacity factor

```
1 // Example 4.4
2 clear all;
3 clc;
4
5 // Given data
6 ratpower = 1075; // Output rated
        electrical power in MWe of the reactor
```

```
7 delpower_yr = 255000;
                                 // Net output power
     delivered in one year in terms of MWd
8 time_refuel = 28;
                                   // Number of days
     the plant was shutdown for refuelling
9 time_repairs = 45;
                                  // Number of days
     the plant was shutdown for repairs
10 time_convrepairs = 18;
                           // Number of days
     the plant was shutdown for conventional repairs
11
12 // 1.
13 // 1 year = 365 days
14 ratpower_yr = ratpower*365; // Net output rated
      power in one year in terms of MWd
15 // Calculation
16 cap_factor = delpower_yr/ratpower_yr;
17 // Result
18 printf(" \n Plant capacity factor = \%d percent\n",
     ceil(cap_factor*100));
19
20 / / 2.
21 // Number of days the plant was shutdown in one year
22 total_shutdown = time_refuel+time_repairs+
     time_convrepairs;
23 // Number of days the plant was operable in one year
24 total_operation = 365-total_shutdown;
25 // Calculation
26 ava_factor = total_operation/365;
27 // Result
28 printf(" \n Plant availability factor = \%d percent\n
     ",ava_factor*100);
```

Scilab code Exa 4.5 Nuclear fuel utilization

```
1 // Example 4.5
2 clear all;
```

```
3 \, \text{clc};
4
5 // Given data
6 t = 30;
                                     // Time of uranium
      sufficiency in years
7 // Assuming once through Light Water Reactor (LWR)
      fuel cycle
8 \text{ U}_{LWR} = 0.0055;
                                     // Uranium
      Utilization factor for LWR
  // Assuming once through Liquid Metal cooled Fast
9
      Breeder Reactor (LMFBR) fuel cycle
                                      // Uranium
10 \ U_LMFBR = 0.67;
      Utilization factor for LMFBR
11 // Estimation
12 est_time = 30*U_LMFBR/U_LWR;
13 // Result
14 printf("The time for which Uranium would fuel LMFBR
     = \%d years \n",ceil(est_time));
```

Scilab code Exa 4.6 Separative work

```
1 // Example 4.6
2 clear all;
3 \text{ clc};
4
5 // Given data
6 \quad A_U = 238;
                              // Atomic Mass number of
      Uranium
7 A_0 = 16;
                              // Atomic Mass number of
      Oxygen
8 \text{ amt}_{U02} = 33000;
                              // Amount of Uranium dioxide
      (UO2) present in kilogram(kg)
                              // Enrichment of 3.2 w/o
9 x_P = 0.032;
      uranium product
10 x_T = 0.002;
                              // Enrichemnt of 0.2 w/o
```

```
residual tails
11 // From Figure 4.45
12 \text{ x}_F = 0.00711;
                            // Enrichemnt of 0.711 w/o
      feed
13
14 // 1.
15 // Estimation of enriched uranium in kg
16 M_P = A_U * amt_UO2/(A_U+2*A_O);
17 // Estimation of amount of Uranium feed in kg
18 M_F = ((x_P-x_T)/(x_F-x_T))*M_P;
19 // Result
20 printf(" \  The amount of uranium feed required per
      reload = \%d kg \n", ceil(M_F));
21
22 / / 2.
                                                  // Value
23 V_x_P = (1-2*x_P)*log((1-x_P)/x_P);
       function of uranium product with enrichemnt of
      3.2 \text{ w/o}
24 V_x_F = (1-2*x_F)*log((1-x_F)/x_F);
                                                  // Value
       function of feed with enrichemnt of 0.711 w/o
                                                  // Value
25 V_x_T = (1-2*x_T)*log((1-x_T)/x_T);
       function of tallings with enrichemnt of 0.2 w/o
26 \text{ rate}_SWU = 130.75;
                                                  Enrichment cost in dollars per SWU
27 // Calculation
28 \quad SWU = M_P * (V_x_P - V_x_T) - M_F * (V_x_F - V_x_T);
                                                  11
      Separative Work (SWU) in kg
29 enrich_cost = ceil(SWU)*rate_SWU;
                                                  //
      Enrichment cost in dollars
30 // Result
31 printf("\n The enrichment cost =  d \in \mathbb{Z}
      enrich_cost));
32 // Due to approximation of Separative Work Unit(SWU)
      , there is a difference in the value of
      enrichment cost on comparison with the textbook
      value.
```

Chapter 5

Neutron Diffusion and Moderation

Scilab code Exa 5.2 Neutron diffusion

```
1 // Example 5.2
2 clear all;
3 \, \text{clc};
4
5 // Given data
6 // 1 \text{ barn} = 10^{(-24)} \text{ cm}^2
7 \text{ sigma_s} = 4.8 \times 10^{(-24)}
                                         // Scattering cross
      section of carbon in cm^2
                                         // Atomic Mass
8 A_C = 12;
      number for \operatorname{carbon} -12
9 = 1;
                                         // Energy of carbon
      -12 atom in eV
10 // Using the data given in Table II.3, for carbon (
      graphite) at energy 1 eV
11 N = 0.08023 \times 10^{(24)};
                                         // Atom density in
      terms of atom/cm<sup>3</sup>
                                         // Average value of
12 mu_bar = 2/(3*A_C);
      the cosine of the angle at which neutrons are
      scattered in the med/ium
```

```
13 SIGMA_s = N*sigma_s // Macroscopic
scattering cross section of carbon-12
14 // Calculation
15 D = 1/(3*SIGMA_s*(1-mu_bar));
16 // Result
17 printf('\n Diffusion coefficeint of graphite at 1 eV
= %4.3 f cm \n',D);
```

Scilab code Exa 5.5 Multigroup diffusion theory

```
1 // Example 5.5
2 clear all;
3 \text{ clc};
4
5 // Given data
6 \text{ phi1} = 6*10^{(14)};
                                         // Neutron flux of
      Group 1
                                         // Neutron flux of
7 phi2 = 1*10^{(15)};
      Group 2
8 \text{ phi3} = 3*10^{(15)};
                                         // Neutron flux of
      Group 3
9
10 // 1.
11 // Using the data given in Table II.3, for atom
      density of sodium
12 \text{ N} = 0.02541 * 10^{(24)};
                                         // Atom density in
      terms of atom/cm<sup>3</sup>
13 // Using the data given for sigmay (Microscopic
      radiative capture cross section) in Table II.3,
14 / / 1 \text{ barn} = 10^{(-24)} \text{ cm}^2
15 \text{ sigmay1} = 0.0005 * 10^{(-24)};
                                         // Microscopic gamma
       cross section of Group 1
16 \text{ sigmay2} = 0.001 * 10^{(-24)};
                                         // Microscopic gamma
        cross section of Group 2
17 \text{ sigmay3} = 0.001*10^{(-24)};
                                         // Microscopic gamma
```

```
cross section of Group 3
18 // Calculation
19 F_a = N*((sigmay1*phi1)+(sigmay2*phi2)+(sigmay3*phi3
      ));
20 // Result
21 printf('\n Total absorption rate for three groups =
      \%3.2E neutrons/cm<sup>3</sup>-sec \n', F_a);
22
23 / / 2.
24 // Calculation
25 sigmag_12 = 0.24*10<sup>(-24)</sup>; // Microscopic
      scattereing cross section of neutrons from Group
      1 to Group 2
26 F_12 = N*sigmag_12*phi1;
27 // Result
28 printf('\n Neutron scattering rate from the first to
       second group = \%3.2E neutrons/cm<sup>3</sup>-sec \n',F_12)
      ;
```

Scilab code Exa 5.6 Neutron diffusion

```
1 // Example 5.6
2 clear all;
3 \text{ clc};
4
5 // Given data
6 S = 10^{7};
                         // Strength of neutron source
    in neutrons/sec
7 r = 15;
                          // Distance over which neutron
      flux is to be calculated in cm
8 // Using the data given in Table 5.2,
9 L_T = 2.85;
                     // Thermal diffusion length in
      cm
10 D_bar = 0.16;
                         // Diffusion coefficient in cm
11 // Calculation
```

```
12 phi_T = S*exp(-r/L_T)/(4*%pi*D_bar*r);
13 // Result
14 printf('\n Neutron flux = %3.2E neutrons/cm^2-sec \n
',phi_T);
```

Scilab code Exa 5.7 Neutron diffusion

```
1 // Example 5.7
2 clear all;
3 \text{ clc};
4
5 // Given data
6 T_F = 500;
                                  // Temeperature in
      Fahrenheit
7 P = 2000;
                                  // Pressure in psi
                                  // Density in terms of
8 \text{ rho} = 49.6;
      lb/ft^3
9 // Converting the given temperature from Fahrenheit
      to Celsius
10 T_C = (5/9) * (T_F - 32);
11 // Converting the temperature from Celsius to Kelvin
       scale
12 T_K = 273 + T_C;
13
14 // Using the data given in Table 5.2,
15 D_bar_0 = 0.16;
                                  // Diffusion coefficient
       at 293 K
16 \text{ rho}_0 = 62.4;
                                  // Density at 293 K in
      terms of lb/ft^3
17 L_T2_0 = 8.1;
                                  // Diffusion area at 293
      K in cm<sup>2</sup>
18 T_0 = 293;
                                  // Standard Temperature
      in kelvin
                                  // Material specific
19 m = 0.47;
      constant
```

- 20 // Calculation
- 21 $D_bar = D_bar_0*(rho_0/rho)*(T_K/T_0)^m;$
- 22 L_T2 = L_T2_0*(rho_0/rho)^2*(T_K/T_0)^(m+1/2);
- 23 // Result
- 24 printf('\n Diffusion coefficient of ordinary water = $\%4.3 \text{ f cm } \text{ (n', D_bar);}$

Chapter 6

Neutron Reactor Theory

Scilab code Exa 6.1 Critical neutron parameters

```
1 // Example 6.1
2 clear all;
3 \, \text{clc};
4
5 // Given data
                                  // Atomic mass of
6 M_F = 235;
     Uranium - 235
7 M_S = 23;
                                  // Atomic mass of Sodium
      -23
8 \text{ rho}_F_S = 1;
                                  // Ratio of densities of
       Uranium fuel to Sodium
9 // Using the data given in Table 5.2,
10 sigmaa_S=0.0008;
                                 // Absorption cross
      section of Sodium
                                  // Absorption cross
11 sigmaa_F=1.65;
      section of Uranium
12
13 \text{ rho}_S_F = 100 - \text{rho}_F_S;
14 N_S_F = rho_S_F*(M_F/M_S); // Ratio of atomic
      densities of Uranium and Sodium
15 // Using the data in Table 6.1 for Uranium -235
```

```
16 // The value of average number of neutrons produced
	for a neutron absorbed n(eta) for Uranium-235 is
	2.2
17 eta = 2.2;
18
19 // Calculation
20 f = 1/(1+(N_S_F*(sigmaa_S/sigmaa_F)));
21 k_inf = eta*f;
22 // Result
23 printf('\n Thermal Utilization factor = %.3f \n',f);
24 printf('\n Infinite Multiplication factor = %3.2f \n
	',k_inf);
```

Scilab code Exa 6.2 Maximum and average flux

```
1 // Example 6.2
2 clear all;
3 \text{ clc};
4
5 // Given data
6 R = 50;
                                // Radius of reactor core
     in cm
7 P = 100 * 10^{6};
                                // Power level of the
      reactor in watt
8 \text{ SIGMA_f} = 0.0047;
                                // Macroscopic fission
      cross section in \operatorname{cm}(-1)
9 E_R = 3.2*10^{(-11)};
                                // Energy released per
      fission in joules/second
10 // Using the data in Table 6.2 for spherical
      geometry
11 OMEGA = 3.29;
                                // Measure of the
      variation of flux in the reactor
12 // Calculation
13 phi_max = (%pi*P)/(4*E_R*SIGMA_f*R^3);
14 phi_av = phi_max/OMEGA;
```

Scilab code Exa 6.3 Critical radius

```
1 // Example 6.3
2 clear all;
3 \, \text{clc};
4
5 // Given data
6 \text{ N}_F = 0.00395 * 10^{(24)};
                                               // Atom
      density of Plutonium-239 fuel in atom/cm<sup>3</sup>
7 \text{ N}_{S} = 0.0234 * 10^{(24)};
                                               // Atom
      density of Sodium-23 in atom/cm<sup>3</sup>
8 // Using the data given in Table 6.1,
9 // 1 barn = 10^{(-24)} cm<sup>2</sup>
10 sigmaa_S = 0.0008*10^(-24);
                                               // Microscopic
       absorption cross section of Sodium in cm<sup>2</sup>
11 sigmaa_F = 2.11*10^{(-24)};
                                               // Microscopic
       absorption cross section of Plutonium in cm<sup>2</sup>
12 sigmatr_F = 6.8*10^{(-24)};
                                               // Microscopic
       transport cross section of Plutonium
13 sigmatr_S = 3.3*10^{(-24)};
                                               // Microscopic
       transport cross section of Sodium
14 // The value of average number of neutrons produced
      for a neutron absorbed n(eta) for Plutonium -239
      is 2.61
15 \text{ eta} = 2.61;
16
  SIGMAA_S = sigmaa_S*N_S;
                                              // Macroscopic
17
      absorption cross section of Sodium in cm^{(-1)}
18 SIGMAA_F = sigmaa_F*N_F;
                                             // Macroscopic
```

```
absorption cross section of Plutonium in cm^{(-1)}
19 SIGMAA = SIGMAA_S+SIGMAA_F;
                                          // Total
      macroscopic absorption cross section in cm^{(-1)}
  SIGMA_tr = (sigmatr_F*N_F)+(sigmatr_S*N_S); //
20
      Macroscopic transport cross section
21 f = SIGMAA_F/SIGMAA;
                                          // Calculation
      of Thermal Utilization factor(f)
22 f = ceil(f);
23 \text{ k_inf} = \text{eta*f};
                                           // Calculation
      of Infinite Multiplication factor(k_inf)
24
25 D = 1/(3*SIGMA_tr);
                                          // Calculation
      of Diffusion coefficient
26 L2 = D/SIGMAA;
                                          // Diffusion
     area
27 d = 2.13 * D;
                                          // Extrapolated
      distance
  R_ctil = %pi*sqrt(L2/(k_inf-1));
                                          // Critical
28
      Radius for an extrapolated boundary
29 // Calculation
30 R_c = R_ctil-d;
31 // Result
32 printf('\n Critical Radius = \%2.1 \text{ f cm \n', R_c};
33 // The answer given in the textbook is wrong.
```

Scilab code Exa 6.4 Non leakage probability

Scilab code Exa 6.5 Critical parameter calculations

```
1 // Example 6.5
2 clear all;
3 \text{ clc};
4
5 // Given data
6 R = 100;
                                        // Radius of a
      spherical reactor in cm
7 P = 10^{5};
                                       // Power of the
      reactor in watt
8
9 // 1.
10 // Calculation
11 B = sqrt((%pi/R)^2);
12 // Result
13 printf (" \  \  Buckling = \%3.2E \ n", B);
14
15 / / 2.
16 // Using the data from Tables 3.2, 5.2, 5.3 and 6.3
17 L_TM2 = 3500;
                                       // Diffusion area of
      moderator (Sodium) in cm<sup>2</sup>
                                       // Average number of
18 n_T = 2.065;
      fission neutrons emitted per neutron absorbed
19 t_TM = 368;
                                      // Diffusion time of
      moderator (Sodium) in cm<sup>2</sup>
20 / / 1 \text{ barn} = 10^{(-24)} \text{ cm}^2
21 \text{ sigma_aM} = 0.0034*10^{(-24)};
                                      // Microscopic
```

absorption cross section of Sodium in cm² $22 \text{ sigma_aF} = 681*10^{(-24)};$ // Microscopic absorption cross section of Uranium -235 in cm² // Non 1/v factor $23 \text{ g_a} = 0.978;$ $24 M_F = 235;$ // Molecular weight of Uranium – 235 $25 M_M = 12;$ // Molecular weight of Carbon - 12 $26 \ Z = (1+B^2*(L_TM2+t_TM))/(n_T-1-(B^2*t_TM)); // An$ intermediate factor 27 // Calculation // Density of Graphite $28 \text{ rho}_M = 1.6;$ in g/cm^3 29 m_M = (4/3*%pi*R^3)*rho_M; // Mass of moderator 30 // Calculation 31 m_F = ((Z*sigma_aM*M_F)/(g_a*sigma_aF*M_M))*m_M /1000;32 // Result 33 printf("\n Critical mass = $\%2.1 \text{ f kg \n",m_F}$; 3435 / / 3.36 f = Z/(Z+1); // Thermal utilization factor 37 // Calculation $38 \text{ k_inf} = n_T * f;$ 39 // Result 40 printf('\n Infinite Multiplication factor $(k_{inf}) =$ $\%.2 f \setminus n', k_inf);$ 41 42 / / 4.43 // Calculation $44 L_T2 = (1-f)*L_TM2$ 45 // Result 46 printf("\n Thermal Diffusion area = %d cm² \n",L_T2); 4748 // 5. // Energy per fission $49 \quad \text{E}_R = 3.2*10^{(-11)};$

```
reaction in joules/second
50 \text{ N}_A = 6.02 * 10^{(23)};
                                    // Avogadro number (
      constant)
51 V = (4/3*\%pi*R^3);
                                    // Volume of the
      spherical reactor in cm<sup>3</sup>
52 // Using the data from Tables 3.2
53 \text{ g}_{fF} = 0.976;
                                    // Non 1/v factor
      Uranium - 235 fuel
54 // Using the data from Tables II.2 for Uranium -235
                                   // Microscopic fission
55 \text{ sigma}_f = 582*10^{(-24)};
       cross section for Uranium - 235 in cm^2
   // Macroscopic fission cross section is calculated
56
      as follows
57 SIGMA_f = m_F*N_A*0.886*g_fF*sigma_f*1000/(V*M_F);
58
  // From Table 6.2, the constant A can be calculated
59
      as
60 A = P/(4*(R^2)*E_R*SIGMA_f);
61
62 // The expression for thermal flux is
63 printf(" \n The expression for thermal flux = \%4.3E
      \sin (Br)/r \setminus n^{"}, A);
64 // The maximum value of thermal flux is given at
      distance equal to zero
65 phi_TO = A*B;
66 // Result
67 printf(" The maximum thermal flux = \%4.3E neutrons/
      cm^2 - sec \ \ n", phi_T0);
68 // There is a slight variation in the values of
      diffusion area and constant A as compared from
      the textbook. This is due to approximation of
      values in textbook.
```

Scilab code Exa 6.6 Critical mass

```
1 // Example 6.6
2 clear all;
3 \text{ clc};
4
5 // Given data
6 \text{ rho}_F = 0.0145;
                                 // Density of Uranium-235
      in the mixture in g/cm<sup>3</sup>
                                 // Density of Water in the
7
  rho_M = 1;
       mixture in g/cm<sup>3</sup>
                                 // Molecular weight of
  M_M = 18;
8
      water
                                 // Molecular weight of
9 M_F = 235;
      Uranium -235
10
11 // 1.
12 // The ratio of number of atoms of Uranium -235 to
      water per cc is
13 NF_NM = (rho_F*M_M)/(rho_M*M_F);
14 // Using the data from Tables 3.2
                                // Non 1/v factor of
15 \text{ g}_{aF} = 0.978;
      Uranium-235 fuel
                                 // Non 1/v factor of Water
16 \, \text{g}_aM = 2;
17 // Using the data from Table II.2 for Uranium -235
18 / / 1 \text{ barn} = 10^{(-24)} \text{ cm}^2
19 \text{ sigma}_{aF} = 681*10^{(-24)};
                                // Microscopic absorption
      cross section of Uranium-235 in cm<sup>2</sup>
20 sigma_aM=0.333*10<sup>(-24)</sup>;
                               // Microscopic absorption
      cross section of Hydrogen in cm<sup>2</sup>
  // Using the data form Table 6.3 at temperature = 20
21
       deg
22 n_T = 2.065;
                                 // Average number of
      neutrons produced per neutron absorbed in fission
23 phisig_aF = 0.886*g_aF*sigma_aF;
                                            // Average
      thermal absorption cross-section of fuel
24 phisig_aM = 0.886*g_aM*sigma_aM;
                                            // Average
      thermal absorption cross-sections of moderator
25 Z = (NF_NM)*(phisig_aF/phisig_aM); // Parameter Z
26 f = Z/(Z+1);
                                            // Thermal
```

```
utilization factor of the fuel
27 k_inf = n_T*f;
                                          // Infinite
      multiplication factor
28
29 // From Table 5.2 and 5.3
30 L_TM2 = 8.1;
                                      // Diffusion area in
      \mathrm{cm} ^{2}
31 t_T = 27;
                                      // Neutron age in cm
32 L_T2 = (1-f) * L_TM2;
                                      // Diffusion area of
       fuel moderator mixture
33 M_T2 = L_T2 + t_T;
                                      // Migration area of
       fuel moderator mixture
34 // Buckling can be found as
35 B2 = (k_inf - 1)/M_T2;
36 printf(" \n Using the buckling formula from Table
      6.2 \ln B^2 = (2.405/R)^2 + (pi/H)^2 \ln For minumum
      critical mass H = 1.82R \setminus n");
37 // On solving for R in B^2 = 8.763/R^2
38 R = sqrt(8.763/B2);
39 \text{ H} = 1.82 * \text{R};
40 // Result
41 printf(" \n The dimensions of the cylinder are");
42 printf(" \n Radius of cylinder = \%2.1 f cm \t Height
      of cylinder = \%3.1 f cm \n", R, H);
43
44 // 2.
45 V = %pi*R^{2*H};
                                          // Reactor
      volume (in cc) assuming cylindrical geometry
46 // Calculation
47 m_F = rho_F * V;
48 printf(" \n The critical fuel mass = \%2.1 f kg \n",
      m_F/1000);
49 // There is a slight variation in the values of
      dimensions of cylinder and critical fuel mass as
      compared from the textbook. This is due to
      approximation of values in textbook.
```

Scilab code Exa 6.7 Critical concentration

```
1 // Example 6.7
2 clear all;
3 \, \text{clc};
4
5 // Given data
6 R = 300;
                                  // Radius of the sphere
      in cm
7 M_M = 20;
                                 // Molecular weight of
      heavy water
8 M_F = 235;
                                 // Molecular weight of
      Uranium - 235
9
10 // 1.
11 // Using the data from Table 5.2
                                   // Diffusion coefficient
12 Dbar_r = 0.84;
       of graphite in cm
13 Dbar_c = 0.87;
                                   // Diffusion coefficient
       of heavy water in cm
                                   // Diffusion area of
14 L_TM2 = 9400;
      heavy water in cm<sup>2</sup>
15 L_r = 59;
                                   // Diffusion length of
      graphite in cm
16 // Using the data from Table 3.2
17 \text{ g}_{aF} = 0.978;
                                   // Non 1/v factor
      Uranium - 235 fuel
18 // Using the data from Table II.2 for Uranium -235
19 // 1 barn = 10^{(-24)} cm<sup>2</sup>
20 \text{ sigma_aF} = 681*10^{(-24)};
                                            // Microscopic
      absorption cross section of Uranium -235 in cm<sup>2</sup>
21 \text{ SIGMA}_aM = 9.3*10^{(-5)}*10^{(-24)};
                                            // Macroscopic
      absorption coefficient of Heavy water in cm^{(-1)}
22 N = 0.03323;
                                            // Atomic
```

```
density of heavy water
23 // Let BRcot(BR) = y
24 y = 1-((Dbar_r/Dbar_c)*((R/L_r)+1));
25 // Considering only the first solution, B*R=2.64
26 B = 2.64/R;
27 // Using the data form Table 6.3 at temperature = 20
       deg
28 n_T = 2.065;
                                           // Average
      number of neutrons produced per neutron absorbed
      in fission
29 \quad Z = (1 + (B^{2} + L_TM2)) / (n_T - 1);
                                           // A parameter
30 sigma_aM = sqrt(4/%pi)*SIGMA_aM/N; // Microscopic
      absorption cross section of Heavy water in cm<sup>2</sup>
31 // The ratio of densities of fuel to moderator
32 rho_FM = Z*(M_F*sigma_aM)/(M_M*g_aF*sigma_aF)
                                           // Density of
33 \text{ rho}_M = 1.1;
      Heavy water in g/cm^3
34 // Calculation
35 \text{ rho}_F = \text{rho}_FM*\text{rho}_M;
36 // Result
37 printf(" \n The critical concentration = \%.4 f g/
      litre \n", rho_F * 1000;
38
39 / / 2.
40 V = (4/3) * \% pi * R^3;
                                           // Reactor
      volume (in cc) assuming spherical geometry
41 // Calculation
42 m_F = rho_F * V;
43 // Result
44 printf(" \n The critical fuel mass = \%3.2 f kg \n",
      m_F/1000);
```

Scilab code Exa 6.8 Critical radius

1 // Example 6.8

```
2 clear all;
3 \text{ clc};
4
5 // Given data
6 \text{ rho}_F = 2*10^{(-4)};
                                     // Concentration of
      Uranium -235 fuel in g/cm<sup>3</sup>
                                     // Concentration of
7
  rho_M = 1.6;
      graphite moderator in g/cm<sup>3</sup>
8 M_F = 235;
                                     // Molecular mass of
      Uranium-235 fuel
                                     // Molecular mass of
9 M_M = 12;
      Graphite (Carbon) moderator
10
11 // 1.
12 // Using the data from Tables 3.2
13 \text{ g}_{aF} = 0.978;
                                     // Non 1/v factor
      Uranium-235 fuel
14 // Using the data from Table II.2 for Uranium -235
      and Carbon
15 / / 1 \text{ barn} = 10^{(-24)} \text{ cm}^2
                                // Microscopic
16 sigma_aF = 681*10^(-24);
      absorption cross section of Uranium-235 in cm<sup>2</sup>
17 sigma_aM = 3.4*10^(-3)*10^(-24); // Microscopic
      absorption cross section of Graphite in cm<sup>2</sup>
18 Z = (rho_F*M_M*g_aF*sigma_aF)/(rho_M*M_F*sigma_aM);
          // Parameter Z
19 f = Z/(Z+1);
                                        // Thermal
      utilization factor of the fuel
  // Using the data form Table 6.3 at temperature = 20
20
       deg
21 n_T = 2.065;
                                       // Average number of
       neutrons produced per neutron absorbed in
      fission
22 k_inf = n_T * f;
                                       // The infinite
      multiplication factor
23 // From Table 5.2
24 L_TM2 = 3500;
                                       // Diffusion area of
       Graphite in cm<sup>2</sup>
```

```
// Diffusion length
25 L_r = 59;
      of graphite in cm
26 L_T2 = (1-f)*L_TM2;
                                       // Diffusion area of
       fuel moderator mixture
27 // Buckling can be found as
28 B = sqrt((k_inf - 1)/L_T2);
29 // Calculation
30 R = acot(-1/(B*L_r))/B;
31 // Result
32 printf(" \n The critical radius of fuel loaded
      thermal reactor = \%3.2 \text{ f cm } \text{n}^{\circ}, \text{R};
33
34 // 2.
35 // Reactor is bare or reflector is not present
36 // Calculation
37 \text{ RO} = \% \text{pi/B};
38 // Result
39 printf(" \n The critical radius of bare thermal
      reactor = \%d cm \n", RO);
40 // There is a slight variation in the value of
      critical radius as compared from the textbook.
      This is due to approximation of the thermal
      utilization factor value in textbook.
```

Scilab code Exa 6.9 Critical radius and mass

```
1 // Example 6.9
2 clear all;
3 clc;
4 
5 // Given data
6 rho_F = 0.0145; // Concentration of
Uranium-235 fuel in g/cm<sup>3</sup>
7 // Using the result of Example 6.6
8 M_T2 = 30.8; // Migration area in
```

```
\mathrm{cm}^2
9 B = 0.0529;
                                     // Buckling factor
10 delta = 7.2+0.1*(M_T2-40);
                                     // Empirical formula
      for reflector savings
11 RO = %pi/B;
                                     // The radius of the
      bare reactor
12 // Calculation
13 R = RO-delta;
14 m_F=rho_F*4/3*%pi*R^3;
15 // Result
16 printf(" \n The critical radius of reflected reactor
      = %3.2 f cm \n",R);
17 printf(" \n The critical mass of reflected reactor =
       \%3.2 f kg \ n",m_F/1000);
```

Scilab code Exa 6.10 Critical parameters for heterogenous reactor

```
1 // Example 6.10
2 clear all;
3 \text{ clc};
4
5 // Given data
6 N = 150;
                                 // Number of zirconium
     atoms for every uranium atom
7
8 // 1.
9 // Using the data of atom density of zirconium from
     Table II.3
10 N_Z = 0.0429;
                                   // Atom density of
      zirconium in terms of 10<sup>(24)</sup>
11 sigma_tZ = 6.6;
                                   // Total cross section
      of zirconium in barns
12 // Using the data of cross section of uranium -235
     from Table II.3
                                   // Total cross section
13 sigma_tU = 690;
```

```
of uranium in barns
14 N_25 = N_Z/N;
                                    // Atom concentration
      of uranium - 235
15 // Calculation
16 lambda = 1/((sigma_tZ*N_Z)+(sigma_tU*N_25));
17 // Result
18 printf(" \n The mean free path of thermal neutrons =
       \%3.1 \, \text{f} \, \text{cm} \, \backslash \text{n}",lambda);
19
20 / / 2.
21 // Using the data of atom density of water from
      Table II.3
22 N_W = 0.0334;
                                    // Atom density of
      water in terms of 10^{(24)}
  // As the water and zirconium occupy half of the
23
      volume
24 N_W = 0.5 * 0.0334;
25 N_Z = 0.5 * 0.0429;
26 // From the Figure 6.6
27 // Uranium is present in one third of the sandwich
      or \n one sixth of the entire area
28 N_{25} = 2.86*10^{(-4)}/6;
29 // Using the data from Table 3.2
30 \text{ g_aF} = 0.978;
                               // Non 1/v factor Uranium
      -235 fuel
31 // Using the data from Table II.3 for microscopic
      absorption cross section
                               // Microscopic absorption
32 sigma_aU = 681;
      cross section of Uranium-235 in barns
33 \text{ sigma_aZ} = 0.185;
                               // Microscopic absorption
      cross section of Zirconium in barns
34 \text{ sigma_aW} = 0.664;
                               // Microscopic absorption
      cross section of Water in barns
35 f = (N_25*g_aF*sigma_aU)/((N_25*g_aF*sigma_aU)+(N_Z*
      sigma_aZ)+(N_W*sigma_aW)); // Thermal
      utilization factor
36 // Using the data form Table 6.3 at temperature = 20
       deg
```

Scilab code Exa 6.11 Critical parameter for heterogenous reactor

```
1 // Example 6.11
2 clear all;
3 \text{ clc};
4
5 // Using the data from Table 3.2
6 g_a25=0.978;
                 // Non 1/v factor Uranium
     -235 fuel for absorption
  g_f 25 = 0.976;
                             // Non 1/v factor Uranium
7
     -235 fuel for fission
                             // Non 1/v factor Uranium
8 g_a28=1.0017;
     -238 fuel for absorption
9
                             // Average number of
10 v_25=2.42;
     neutrons in one fission of Uranium-235
11 // Using the data from Table II.3 for microscopic
      absorption and fission cross section
                            // Microscopic absorption
12 sigma_a25=681;
      cross section of Uranium -235 in barns
13 sigma_a28=2.7;
                            // Microscopic absorption
      cross section of Uranium-238 in barns
                             // Microscopic fission
14 sigma_f25=582;
      cross section of Uranium-235 in barns
15
16 // Using the data of atom density of uranium and let
      N_{28}/N_{25} = N
```

```
17 N = 138;
18 // Calculation
19 n_T = (v_25*sigma_f25*g_f25)/((sigma_a25*g_a25)+(N*
sigma_a28*g_a28));
20 // Result
21 printf("\n Average number of neutrons produced per
neutron absorbed in fission = %3.2f \n",n_T);
```

Scilab code Exa 6.12 Critical parameter for heterogenous reactor

```
1 // Example 6.12
2 clear all;
3 \text{ clc};
4
5 // Given data
                                        // Distance
6 \text{ rdist} = 25.4;
      between the rods in cm
7 a = 1.02;
                                        // Radius of a rod
      in cm
8 // From the Figure 6.9
9 b = rdist/sqrt(%pi);
                                       // Radius of
     equivalent cell in cm
10 // Using the data from Table 5.2
11 L_F = 1.55;
                                       // Diffusion length
      of uranium fuel in cm
12 L_M = 59;
                                       // Diffusion length
       of graphite moderator in cm
13 // Using the data from Table II.3 at thermal energy
14 \text{ SIGMA}_aM = 0.0002728;
                                     // Macroscopic
      absorption cross section of graphite moderator in
       barns
15 \text{ SIGMA}_aF = 0.3668;
                                      // Macroscopic
      absorption cross section of uranium fuel in barns
16 // Let
17 x = a/L_F;
```

18 y = a/L_M ; 19 $z = b/L_M;$ 20 // The series expansion relations are 21 F = $1+(0.5*(x/2)^2) - ((1/12)*(x/2)^4) + ((1/48)*(x/2))$ $^{6};$ 22 E = $1+(z^2/2)*(((z^2*\log(z/y))/(z^2-y^2))-(3/4)+(y)$ ^2/(4*z^2))); 23 // Let the ratio of volumes of moderator to fuel is denoted by V $24 V = (b^2 - a^2) / a^2;$ 25 // Calculation 26 f = $1/((SIGMA_aM*V*F/SIGMA_aF)+E);$ 27 // Result 28 printf("\n The thermal utilization factor = %.4 f \n" .f); 29 // There is a slight variation in the value as compared from the textbook. This is due to approximation of the parameters value in textbook

Scilab code Exa 6.13 Critical parameter for heterogenous reactor

1 // Example 6.13 2 clear all; $3 \, clc;$ 4 5 // Using the data given in the problem 6.126 rdist = 25.4;// Distance between the rods in cm 7 a = 1.02;// Radius of the rod in cm 8 b = rdist/sqrt(%pi); // Radius of equivalent cell $9 V = (b^2 - a^2) / a^2;$ // Ratio of volumes of moderator to fuel

```
10 // Using the data from Table II.3 for Uranium -238
      density and atom density
                                             // Uranium-238
11 rho = 19.1;
       density in g/cm<sup>3</sup>
12 N_F = 0.0483;
                                             // Atom
      density in terms of 10^{(24)}
13 // Using Table 6.5 for Uranium -238
14 \quad A = 2.8;
15 C = 38.3;
16 // Using Table 6.6 for graphite
17 // Let zeta_M*SIGMA_sM = s
18 \ s = 0.0608;
19 I = A+C/sqrt(a*rho);
                                             // Empirical
      expression of resonance integral parameter
20 // Calculation
21 p = \exp(-(N_F*I)/(s*V));
22 // Result
23 printf("\n Resonance escape probability = \%.4 \text{ f} \n",p
      );
```

Chapter 7

The Time Dependent Reactor

Scilab code Exa 7.1 Reactor kinetics

```
1 // Example 7.1
2 clear all;
3 \text{ clc};
4
5 // Using the data form Table 6.3 at temperature = 20
       deg
6 n_T = 2.065;
                               // Average number of
      neutrons produced per neutron absorbed in fission
7 // Using the data from Table 7.1
8 t_dM = 2.1e-4;
                               // The mean diffusion time
       of the moderator in seconds
9 k_{inf} = 1;
                               // The reactor is critical
10 f = k_inf/n_T;
                               // Thermal utilization
      factor
11 // Calculation
12 t_d = t_dM*(1-f);
13 l_p = t_d;
14 // Result
15 printf(" \n The prompt neutron lifetime = \%3.2E
      seconds \langle n, l_p \rangle;
```

Scilab code Exa 7.2 Reactor period

```
1 // Example 7.2
2 clear all;
3 \text{ clc};
4
5 // Given data
6 \text{ k_inf} = 1.001;
                                              // Infinite
       multiplication factor
7 // From the Example 7.1
                                              // Prompt
8 l_p = 1e-4;
      neutron lifetime
9 // Calculation
10 T = l_p/(k_{inf}-1);
11 // Result
12 printf(" \n The response time of the reactor = \%2.1 f
       sec \langle n^{"}, T \rangle;
13 printf(" \n The reactor power will increase as exp(t
      /\%2.1\,{
m f}), where 't'' denotes the time in seconds
      \langle n, T \rangle;
```

Scilab code Exa 7.3 Reactivity

```
1 // Example 7.3
2 clear all;
3 clc;
4 
5 // Given data
6 k_inf = 1.001;
multiplication factor
7 // Calculation
8 rho = (k_inf-1)/k_inf;
```

```
// Infinite
```

Scilab code Exa 7.4 Reactor period

```
1 // Example 7.4
2 clear all;
3 clc;
4
5 // Using the result of Example 7.1
6 lp = 1e-4; // Prompt neutron
lifetime in seconds
7 // Using the result of Example 7.3
8 rho = 1e-3; // Reactivity
9 // By referring to Figure 7.2
10 printf(" \n Reactor period = 57 seconds \n");
```

Scilab code Exa 7.5 Reactivity

```
1 // Example 7.5
2 clear all;
3 clc;
4
5 // Using the result of Example 7.3
6 reactivity = 0.001;
7 // As the reactor is fueled with Uranium-235
8 bet = 0.0065; // Total delayed
neutron fraction of all groups denoted by 'beta'
9 printf(" \n A dollar is worth 0.0065 in reactivity
for Uranium-235 reactor. \n");
10 // Calculation
11 rho = reactivity/bet;
```
```
Scilab code Exa 7.6 Prompt drop
```

```
1 // Example 7.6
2 clear all;
3 \text{ clc};
4
5 // Given data
6 PO = 500;
                                          // Reactor power
      in MW
7 rho = -0.1;
                                          // 10% in
      reactivity (Insertion of control rods correspond
      to negative reactivity)
8 // As the reactor is fueled with Uranium -235
9 bet = 0.0065;
                                          // Total delayed
      neutron fraction of all groups denoted by 'beta'
10
11 P1 = (bet*(1-rho)*P0)/(bet-rho); // The drop in
      power level in terms of MW
12 // Assuming that negative reactivity is greater than
      4%
13 T = 80;
                                          // Reactor
      period obtained from Figure 7.2 in seconds
14 t = 600;
                                          // Analysis time
      in seconds
15 // Calculation
                                          // Power level
16 P = P1 * exp(-t/T);
      drop in MW
17 // Result
18 printf(" \n The power level drop after 10 minutes =
     \%5.4 \text{ f MW} \setminus \text{n",P};
```

Scilab code Exa 7.7 Control worth of a center rod

```
1 // Example 7.7
2 clear all;
3 \, \text{clc};
4
5 // Given data
6 H = 70;
                                                       //
      Height of the cylinder in cm
7 R = H/2;
                                                       //
      Diameter of the cylinder in cm
8 a = 1.9;
                                                       11
      Radius of black control rod in cm
9 // From Table 6.2, Buckling can be found by
10 B0 = sqrt((2.405/R)^2+(%pi/H)^2);
11 // Using the data from Table 5.2 and 5.3
12 L_TM2 = 8.1;
                                                       //
      Diffusion area of water moderator in cm<sup>2</sup>
13 t_TM = 27;
                                                       //
      Neutron age of water moderator in cm<sup>2</sup>
14 // Using the data form Table 6.3 at temperature = 20
       deg
15 n_T = 2.065;
      Average number of neutrons produced per neutron
      absorbed in fission
16 // Using the data from Table 5.2 and Table II.3
17 \text{ D}_{bar} = 0.16;
                                                       //
      Thermal neutron diffusion coefficient in cm
18 \text{ SIGMA_t} = 3.443;
                                                       //
      Total macroscopic cross section in cm^{(-1)}
19 f = (1+B0^{2}(L_TM2+t_TM))/(n_T+B0^{2}L_TM2);
                                                       //
      Thermal utilization factor
20 \text{ M}_T2 = (1-f) * L_TM2 + t_TM;
                                                       //
      Thermal migration area in cm<sup>2</sup>
```

```
21 d = 2.131*D_bar*(a*SIGMA_t+0.9354)/(a*SIGMA_t
+0.5098); // Extrapolation distance
22 // Calculation
23 rho_w = (7.43*M_T2*(0.116+log(R/(2.405*a))+(d/a))
^(-1))/((1+B0^2*M_T2)*R^2);
24 // Result
25 printf(" \n The worth of a black control rod = %.3f
or %2.1f percent \n",rho_w,rho_w*100);
```

Scilab code Exa 7.8 Total control rod worth

```
1 // Example 7.8
2 clear all;
3 \, \text{clc};
4
5 // Using the data and result from Example 7.7
6 f = 0.583;
                                                  11
      Thermal Utilization factor
                                                  //
7 L_TM2 = 8.1;
      Diffusion area of water moderator in cm<sup>2</sup>
8 R = 35;
                                                  // Radius
       of the cylinder of the core in cm
9 a = 0.508;
                                                  // Radius
      of control rod in cm
10 Rc = sqrt(R^2/100);
                                                  11
      Critical radius in cm
11 L_T = sqrt((1-f)*L_TM2);
                                                  //
      Thermal diffusion length in cm
12 // The points of estimation are chosen as follows
13 y = a/L_T;
14 z = Rc/L_T;
15 // Using the data given in Table V.I for modified
      Bessel functions
16 \quad I0_{275} = 1.019;
                                                 // I0 at
      0.275
```

// I1 at $17 I1_275 = 0.1389;$ 0.275 $18 \text{ I1}_{189} = 1.435;$ // I1 at 1.89 $19 \text{ KO}_{275} = 1.453;$ // K0 at 0.275 $20 \text{ K1}_275 = 3.371;$ // K1 at 0.275 $21 \text{ K1}_{189} = 0.1618;$ // K1 at 1.89 22 E = $((z^2-y^2)/(2*y))*(((I0_275*K1_189)+(K0_275*$ I1_189))/((I1_189*K1_275)-(K1_189*I1_275))); // The lattice function 23 // Using the data from Table 5.2 and Table II.3 $24 D_bar = 0.16;$ // Thermal neutron diffusion coefficient in cm // Total $25 \text{ SIGMA_t} = 3.443;$ macroscopic cross section in $cm^{(-1)}$ 26 d = 2.131*D_bar*(a*SIGMA_t+0.9354)/(a*SIGMA_t +0.5098); // Extrapolation distance 27 $f_R = 1/((((z^2-y^2)*d)/(2*a))+E);$ // Rod utilization parameter 28 // Calculation 29 $rho_w = f_R/(1-f_R);$ 30 // Result 31 printf(" \n The total worth of the control rods = %.3 f or %2.1 f percent n, rho_w, rho_w*100); 32 // There is a deviation in the value computed on comparison with the value given in the textbook. This is due to approximation of thermal diffusion area in the textbook.

Scilab code Exa 7.9 Total control rod worth

```
1 // Example 7.9
2 clear all;
3 \text{ clc};
4
5 // Given data
6 SIGMAa_bar = 0.2;
      Average macroscopic absorption cross section in
      cm^{(-1)}
7 L_T = 1.2;
                                                        11
      Thermal diffusion length in cm
8 // Converting the given dimensions from inches to
      centimeters
9 / / 1 inch = 2.54 cm
10 // From Figure 7.9
                                                       11
11 1 = 9.75*(2.54/2);
      Length of the half rod
12 a = 0.312*(2.54/2);
                                                       11
      Thickness of the half rod
13 \text{ m} = 44.5/\text{sqrt}(2);
                                                       //
      Closest distance between two rods
14
15 D_bar = SIGMAa_bar*L_T^2;
                                                        //
      Thermal neutron diffusion coefficient in cm
16 \, d = 2.131 * D_{bar};
                                                        //
      Extrapolation distance in cm which is obtained
      for bare planar surface
17 f_R = ((4*(1-a)*L_T)/(m-(2*a))^2*(1/((d/L_T)+coth)(m-(2*a)))^2*(1/((d/L_T)+coth)))^2*(1/((d/L_T)+coth))^2
      -(2*a))/(2*L_T)))); // Rod utilization
      parameter
18 // Calculation
19 rho_w = f_R/(1-f_R);
20 // Result
21 printf(" \n The total worth of the control rods = \%
      .3 f or \%.1 f percent \n", rho_w, rho_w*100);
22 // There is a slight deviation in the value computed
       on comparison with the value given in the
      textbook. This is due to approximation of rod
      utilization parameter in the textbook.
```

Scilab code Exa 7.10 Total control rod worth

1 // Example 7.10 2 clear all; 3 clc;4 5 // Given data $6 \, d = 5;$ // Inner diameter of the tube in cm 7 = d/2;// Inner radius of the tube in cm // Length $8 \ 1 = 76;$ of the tube in cm 9 rho = 2;// Density of B4C in g/cm^3 $10 \ n = 5;$ // Number of rods in the reactor 11 m_B4C = 2*(n*%pi*(a^2)*1); // Mass of B4C in all the rods 12 // Using the data from standard periodic table $13 \text{ molwt}_B = 10.8;$ // Molecular weight of Boron(B)14 $molwt_C = 12;$ // Molecular weight of Carbon(C)15 molwt_B4C = (4*molwt_B)+molwt_C; // Molecular weight of B4C $16 \text{ N}_A = 0.6*10^{(24)};$ // Avogadro number 17 // From Table II.3 $18 \text{ sigma_a} = 0.27*10^{(-24)};$ Microscopic absorption cross section of boron in cm ^2 $19 \ n_B = (4*m_B4C*N_A)/molwt_B4C;$ // Number of boron atoms

```
20 // Using the result of Example 6.3
21 \text{ SIGMA}_aF = 0.00833;
                                                //
      Macroscopic absorption cross section of plutonium
      fuel in cm^{(-1)}
22 \text{ SIGMA}_aC = 0.000019;
                                                //
      Macroscopic absorption cross section of sodium
      coolant in cm^{(-1)}
23 R_c = 41.7;
                                                //
      Critical radius in cm
24 N_B = n_B/((4/3)*\%pi*R_c^3);
                                               // Atom
      density of boron over an entire reactor assuming
      spherical shape
25 SIGMA_aB = sigma_a*N_B;
                                               Macroscopic absorption cross section of boron
26 // Calculation
27 rho_w = SIGMA_aB/(SIGMA_aF+SIGMA_aC);
28 // Result
29 printf(" \n The worth of the control rods using one
     group theory = \%.4 f or \%.2 f percent n, rho_w,
     rho_w*100);
30 // In textbook, the final answer of total worth of
      control rods in percentage is wrong.
```

Scilab code Exa 7.11 Differential control rod worth

```
1 // Example 7.11
2 clear all;
3 clc;
4 
5 // Given data
6 H = 70; //
Height of square cylindrical reactor in cm
7 rho_wH = 0.065; //
Total worth of a control rod at full height
8 rho_wx = 0.01; //
```

```
Total worth of a control rod to be achieved
9 // Let y - \sin(y) = t
10 t = 2*\%pi*(rho_wx/rho_wH);
11 // Using Newton Raphson method for solving the
      transcendental equation y - \sin(y) - 0.966 = 0
12 deff('y=f(y)', 'y = y-sin(y) -0.966')
13 deff('y=f1(y)', 'y = 1 - \cos(y)')
                         // Initial value
14 y0=0.5;
                         // Relative error tolerance
15 e = 0.00001;
16 for i=1:4
       y1 = y0 - f(y0) / f1(y0)
17
18
       e1 = abs(y0-y1)
19
       y0 = y1;
       if abs(y0)<e then</pre>
20
21
            break;
22
       end
23 end
24 y = y1;
                                                         11
      The solution of transcendental equation
25 // Calculation
26 x = (y*H)/(2*\%pi);
27 // Result
28 printf('\n The length of control rod to be inserted
      = \%2.1 \, \text{f} \, \text{cm} \, (n', x);
```

Scilab code Exa 7.12 Chemical Shim

// Thermal

// Total

```
excess reactivity
8 \text{ rho}_w = 0.085;
                                                  // Total
      worth of control rods
                                                  // Total
9 \text{ rho}_{sh} = \text{rho}_{rho}_{w};
      worth of shim control
10 C = (rho_sh*10^3)/(1.92*(1-f0));
                                                  11
      Concentration of boric acid in ppm
11 printf('\n The minimum concentration of boric acid =
       %d ppm \langle n', ceil(C) \rangle;
12 // Expressing in gram/litre
13 // Using the data from standard periodic table
14 \text{ molwt}_B = 10.8;
                                                  //
      Molecular weight of Boron(B)
15 \text{ molwt}_0 = 16;
                                                  //
      Molecular weight of Oxygen(O)
  molwt_H = 1;
16
                                                 ||
      Molecular weight of Hydrogen(H)
17 molwt_H3BO3 = (3*molwt_H)+molwt_B+(3*molwt_0);
                // Molecular weight of Boric acid
18 // Calculation
19 amt_H3B03 = (molwt_H3B03/molwt_B)*C/1000;
20 // Result
21 printf("\n The shim system must contain %3.2 f g/
      litre of boric acid to hold down the reactor. n"
      ,amt_H3BO3);
```

Scilab code Exa 7.13 Temperature coefficient of reactivity

//

```
// Given
7 T = 273 + 350;
      temeprature converted in Kelvin
8 d = 2.8;
                                                  11
     Diameter of rod in cm
9 a = d/2;
                                                  // Radius
      of rod in cm
                                                  // Density
10 rho = 19.1;
       of uranium in g/cm<sup>3</sup>
11 // Using data from Table 7.4 for Uranium -238
12 A = 48 \times 10^{(-4)};
                                                  11
      Constant value
13 C = 1.28 \times 10^{(-2)};
                                                  //
      Constant value
14 beta_I = A+C/(a*rho);
                                                  // A
      parameter
15
16 // Calculation
17 alpha_prompt = -(beta_I/(2*sqrt(T)))*log(1/p);
18 // Result
19 printf('\n The prompt temperature coefficient = \%.2E
       per K \n', alpha_prompt);
```

Scilab code Exa 7.14 Fission product poisons

```
1 // Example 7.14
2 clear all;
3 clc;
4 
5 // Assuming that the fission product poisoning
results in 12 barns per original Uranium-235 atom
in a time frame of one year
6 sigma_p = 12; //
Microscopic poison cross section in barns
7 v = 2.42; // Average
number of neutrons produced in fission
```

```
8 // Using Table II.2 for fission cross section of
Uranium-235 at thermal energy
9 sigma_f = 587; //
Microscopic fission cross section in barns
10 // Calculation
11 rho = -sigma_p/(v*sigma_f);
12 // Result
13 printf(" \n The reactivity due to poisons = %.5f or
%.3f percent \n",rho,rho*100);
```

Chapter 8

Heat Removal from Nuclear Reactors

Scilab code Exa 8.1 Coolant temperature

```
1 // Example 8.1
2 clear all;
3 clc;
4
5 // Given data
6 P = 3025;
                                               // Reactor
       thermal power in MW
7 w = 136.3 * 10^{6};
                                               // Coolant
      flow rate in lb/hr
8 // According to Table 1.9
9 // 1 kW = 3412 Btu/hr
                                              11
10 q = P*1000*3412;
     Converting into Btu/hr
11 delh = q/w;
                                              // Rise in
      enthalpy
12 // Using the data from Table IV.1 for temperature
     542.6 F
                                               //
13 hin = 539.7;
     Enthalpy of input water in Btu/lb
```

```
14 // Calculation
15 hout = hin+delh; //
Enthalpy of released water in Btu/lb
16 // From Table IV.1
17 // Result
18 printf(" \n %3.1f Btu/lb corresponds to 599 F
coolant water temperature. \n",hout);
```

Scilab code Exa 8.2 Steam temperature

```
1 // Example 8.2
2 clear all;
3 \text{ clc};
4
5 // Given data
                                                  11
6 P = 6.895;
      Pressure of steam in MPa
7 w = 2.93 * 10^{6};
                                                  // Steam
      flow rate in kg/hr
8 Tin = 190.6+273;
                                                  // Inlet
      temperature in Kelvin
9
10 // 1.
11 // Using the data from Table IV.2
12 // Result
13 printf(" \n At a pressure of 6.895 MPa the steam
      temeperature is 284.86 \text{ C} \text{ n};
14
15 / / 2.
16 // Using the data from Table IV.2
                                                  //
17 hout = 2773.2;
      Enthalpy of spent steam in kJ/kg
18 // Using the data from Table IV.1
19 hin = 807.8;
                                                   11
      Enthalpy of inlet steam at Tin in k{\rm J}/k{\rm g}
```

Scilab code Exa 8.3 Heat production in fuel rods

```
1 // Example 8.3
2 clear all;
3 \, \text{clc};
4
5 // Given data
6 n = 193 * 204;
                                                // Total
     number of fuel rods in the reactor
7 // 1 feet = 12 inches
                                                // Outer
8 R = 67/12;
     radius of the cylinder in feet(ft)
                                                // Outer
9 H = 144/12;
      radius of the cylinder in ft
10 \ d = 0.42/12;
                                                //
     Diameter of the fuel rod in ft
11 a = d/2;
                                                // Radius
     of the fuel rod in ft
12 P = 1893;
                                                   Reactor
                                                11
       thermal power in MW
13 Ed = 180;
                                                // Energy
      deposited locally in the fuel per fission in MW(
      Assumption)
14 ER = 200;
                                                11
      Recoverable energy per fission in MW(Assumption)
15
16 // 1.
17 // Calculation
18 // According to Table 1.9
```

```
19 // 1 kW=3412 Btu/hr
20 q_r = (2.32*P*Ed)/(n*ER);
21 q_max=(q_r*3412*1000)/(2*H*a^2);
22 // Result
23 printf(" \n Total energy production at the axis = \%
      .2E Btu/hr",(q_r*3412*1000));
24 printf(" \n Maximum energy production at the axis =
     \%.2E Btu/hr-ft^3 \n",q_max);
25
26 / / 2.
27 r = 20/12;
                                                  //
     Distance from the axis in ft
28
  j0 = bessel j(0, ((2.405*r)/R));
                                                 //
      Bessel function
29 // Calculation
30 // According to Table 1.9
31 // 1 kW=3412 Btu/hr
32 q_r20 = q_r*j0;
33 q_max20 = (q_r20*3412*1000)/(2*H*a^2);
34 // Result
35 printf(" \n Total energy production at a distance of
      20 inches = \%.2E Btu/hr", (q_r20*3412*1000));
36 printf(" \n Maximum energy production at a distance
      of 20 inches = \%.2E Btu/hr-ft^3 \n",q_max20);
```

Scilab code Exa 8.4 Decay energy

```
1 // Example 8.4
2 clear all;
3 clc;
4
5 // Given data
6 P0 = 825; //
Reactor thermal power in MW
7 t0 = 1.5*3.16*10^7; //
```

Reactor operation time in seconds 8 ts = 0.1;11 Reactor shutdown time in seconds 9 10 // 1. 11 // Let P/P0 = q12 // From Figure 8.3 $13 \, q_{ts} = 0.07;$ 11 Fission product to decay power during shutdown time $14 q_t0 = 0.0007;$ Fission product to decay power after operating time // Net $15 \, q = q_ts - q_t0;$ fission product to decay power 16 // Calculation 17 P = q * P0;18 // Result 19 printf(" \n Decay energy at shutdown = %2.1 f MW', P); 2021 // One hour after shutdown $22 \text{ ts1} = 3.6*10^3;$ // Reactor shutdown time in seconds 23 // Let P/P0=q 24 // From Figure 8.3 $25 \text{ q_ts1} = 0.014;$ 11 Fission product to decay power at shutdown time $26 q_t0 = 0.0007;$ Fission product to decay power after operating time $27 \ q1 = q_ts1-q_t0;$ 28 // Calculation 29 P1 = q1 * P0;30 // Result 31 printf(" \n Decay energy one hour after shutdown = %2.1 f MW['], P1); 3233 // One year after shutdown

```
34 \text{ ts2} = 3.16*10^7;
                                                        Reactor shutdown time in seconds
35 // Let P/P0=q
36 // From Figure 8.3
37 q_{ts2} = 0.00079;
                                                        11
      Fission product to decay power at shutdown time
38 // Now the operating time is t0+ts2 which can be
      denoted by t01
39 \, q_t01 = 0.00063;
                                                        11
      Fission product to decay power after operating
      time
40 \ q2 = q_ts2-q_t01;
41 // Calculation
42 P2 = q2*P0;
43 // Result
44 printf(" \n Decay energy one year after shutdown = \%
      .3 f MW \setminus n", P2);
45
46 // 2.
47 C = 0.88;
                                                       //
      Conversion factor
48 // Using data from Table II.2
49 \text{ sigma}_a 25 = 681;
                                                       11
      Microscopic absorption cross section in barns
50 \text{ sigma}_{f25} = 582;
                                                       //
      Microscopic fission cross section in barns
51 // At shutdown time
52 P_29 = (2.28*10<sup>(-3)</sup>*C*(sigma_a25/sigma_f25))*P0;
53 P_39 = (2.17*10<sup>(-3)</sup>*C*(sigma_a25/sigma_f25))*P0;
54 printf(" \n Decay energy at shutdown with effect of
      Uranium -239 and Neptunium -239 decay = \%2.2 f MW
      and \%2.2 f MW respectively", P_29, P_39);
55
56 // One hour after shutdown
57 \text{ ts1} = 3600;
                                                       //
      TIme in seconds
58 P_{291} = P_{29*exp}(-4.9*10^{(-4)*ts1});
59 P_391 = P_39*(exp(-3.41*10^{(-6)}*ts1) - (7*10^{(-3)}*exp)
```

 $(-4.9*10^{(-4)}*ts1)));$

60 printf(" \n Decay energy one hour after shutdown
with effect of Uranium-239 and Neptunium-239
decay = %2.2 f MW and %2.2 f MW respectively",P_291
,P_391);

```
61
```

```
62 // One year after shutdown
63 P_292 = 0; //
Half life of Uranium-239 is 23.5 minutes
64 P_392 = 0; //
Half life of Neptunium-239 is 2.35 days
65 printf(" \n Decay energy one year after shutdown
with effect of Uranium-239 and Neptunium-239
decay = %d MW and %d MW respectively", P_292, P_392
);
66 // There is a slight deviation in the values as
compared with the texbook. This is because of
approximation of difference values in the
textbook.
```

Scilab code Exa 8.5 Fuel rod temperature parameters

```
1 // Example 8.5
2 clear all;
3 \, clc;
4
5 // Given data
6 / / 1 feet = 12 inches
7 d = 0.42/12;
                                                11
     Diameter of the fuel rod in feet(ft)
                                                // Radius
8 a = d/2;
     of the fuel rod in ft
9 b = 0.024/12;
                                                11
      Thickness of Zircaloy-4 clad in ft
                                                // Length
10 H = 12;
```

```
of fuel rod in ft
11 T_m = 3970;
                                                 // Center
      temperature of fuel in F
12
13 // 1.
14 // Using the result of Example 8.3
15 \text{ q_max} = 4.66*10^7;
                                                 // Maximum
       heat flux at the center of the rod in Btu/hr-ft
      ^{3}
16 // Calculation
17 q_bar = (a^2*q_max)/(2*(a+b));
18 // According to Table 1.9
19 // 1 kW=3412 Btu/hr
20 // Result
21 printf(" \n Heat flux of the fuel rod = \%.2E Btu/hr-
      ft^2 or \%3.1 \, f \, W/cm^2 \, \langle n, q_bar, (q_bar*1000)
      /(3412*30.48^2));
22
23 / / 2.
24 // Using the data from Table IV.6
                                                 // Thermal
25 k_f = 1.1;
       conductivity of fuel rod in Btu/hr-ft-F
                                                 // Thermal
26 k_c = 10;
       conductivity of cladding in Btu/hr-ft-F
27 R_f = 1/(4*\%pi*H*k_f);
                                                 // Thermal
       resistance of fuel in F-hour/Btu
28 R_c = \log(1+(b/a))/(2*\%pi*H*k_c);
                                                 // Thermal
       resistance of cladding in F-hour/Btu
29 // Calculation
30 T_c = T_m - (q_bar * 2 * \% pi * (a+b) * H * (R_f + R_c));
31 // Result
32 printf(" \n Outer temperature of cladding = \%d F \n"
      ,ceil(T_c));
```

Scilab code Exa 8.6 Coolant temperature

```
1 // Example 8.6
2 clear all;
3 \text{ clc};
4
5 // Given data
6 h = 7500;
                                                     //
     Heat transfer coefficient in Btu/hr-ft^2-F
7 // Using the result of Example 8.5
8 \text{ q_bar} = 3.66*10^{5};
                                                     //
     Heat flux of the fuel rod in Btu/hr-ft^2
9 T_c = 650;
                                                     //
      Outer temperature of cladding in F
10 // Calculation
11 T_b = T_c-(q_bar/h);
12 // Result
13 printf(" \n Temperature of water with respect to the
       midpoint of the hottest fuel rod = \%d F \n", T_b)
      ;
```

Scilab code Exa 8.7 Fuel rod temperature parameters and coolant temperature

```
1 // Example 8.7
2 clear all;
3 \, clc;
4
5 // Given data
6 T_b0 = 543;
                                                   //
      Temperature of inlet coolant in F
                                                  // Coolant
7 w = 3148;
       rate per channel in lb/hr
8
9 // 1.
10 V_f = 1.15*10^{(-2)};
                                                  // Volume
      of fueled portion in ft<sup>2</sup>
```

11 // Using the result of Example 8.3 $12 \, q_max = 4.66*10^7;$ // Maximum heat flux at the center of the rod in Btu/hr-ft 3 13 // From Table IV.3 $14 \ c_p = 1.3;$ // Specific heat at constant pressure in Btu/lb-F 15 // Calculation 16 T_bmax = T_b0+((2*q_max*V_f)/(%pi*w*c_p)); 17 // Result 18 printf(" \n Exit temperature of the coolant = %d F \ n",T_bmax); 1920 / / 2.21 // Using the data of Example 8.6 22 h = 7500;// Heat transfer coefficient in Btu/hr-ft^2-F 23 // Using the data of Example 8.5 $24 \ d = 0.42/12;$ // Diameter of the fuel rod in feet(ft) // Radius $25 \ a = d/2;$ of the fuel rod in ft $26 \ b = 0.024/12;$ // Thickness of Zircaloy-4 clad in ft 27 H = 12;// Length of fuel rod in ft 28 A = 2*%pi*(a+b)*H;// Area of the assumed cylinder in ft^2 29 $R_h = 1/(h*A);$ Convective resistance in F-hour/Btu // A 30 alpha = %pi*w*c_p*R_h; parameter 3132 // Using the result from Example 8.5 $33 R_f = 6.03 * 10^{(-3)};$ // Thermal resistance of fuel $34 \quad R_c = 1.43*10^{(-4)};$ // Thermal resistance of cladding

```
35 R = R_f+R_c+R_h; // Total
resistance
36 bet = %pi*w*c_p*R; // A
parameter denoted by 'beta'
37 // Calculation
38 T_cmax = T_b0+((q_max*V_f*R_h)*((1+sqrt(1+alpha^2))/
alpha));
39 T_mmax = T_b0+((q_max*V_f*R)*((1+sqrt(1+bet^2))/bet))
);
40 // Result
41 printf(" \n Maximum temperature of cladding and fuel
= %d F and %d F respectively. \n",ceil(T_cmax),
T_mmax);
```

Scilab code Exa 8.8 Reynolds number

1	// Example 8.8		
2	clear all;		
3	clc;		
4			
5	// Given data		
6	d = 0.42;	11	
	Diameter of the fuel rod in inches		
$\overline{7}$	b = 0.024;	11	
	Thickness of Zircaloy-4 clad in inches		
8	v = 15.6 * 3600;	11	Speed
	of fluid in feet/hour		
9	a = (d/2) + b;	11	Radius
	of fuel rods in inches		
10	P = 2000;	11	
	Pressure of water in psi	, ,	
11	T = 600;	11	Water
	temperature in F	, ,	
12	// Using the data from example 8.5		
13	s = 0.6;	11	Pitch

```
of square array in inches
14 D_e = 2*((s^2-(%pi*a^2))/(%pi*a));
                                               11
      Equivalent diameter in inches
15 // Converting the units in terms of feet
16 D_e = D_e/12;
17 // Using tha Table IV.3 at given T and P value
18 \text{ rho} = 42.9;
                                                // Density
       of fluid in ft/hr
19 mu = 0.212;
                                                //
      Viscosity of fluid in lb/hr-ft
20 // Calculation
21 Re = (D_e*v*rho)/mu;
22 // Result
23 printf(" \  \  Reylonds number = \  \  d \ n", Re);
24 if Re >= 10000 then
       printf(" \n As the reylonds number is greater
25
          than 10000, the flow is turbulent. n");
26 end
27 // The value is different as compared to the
      textbook value. This is due to approximation of
      Reynolds number in the textbook.
```

Scilab code Exa 8.9 Heat transfer coefficient

9 a = (d/2)+b; // Radius of fuel rods in inches $10 D_e = 0.0427;$ 11 Equivalent diameter in feet 11 Re = 484329; // Reynolds number // The 12 PD = s/(2*a); ratio of pitch to diameter of fuel rod 13 // For a square lattice 14 C = 0.042 * PD - 0.024; // A constant 1516 // According to Table IV.3 $17 \text{ c_p} = 1.45;$ Specific heat at constant pressure in Btu/lb-F 18 mu = 0.212;11 Viscosity of fluid in lb/hr-ft 19 k = 0.296; // Conductivity of fluid in Btu/hr-ft F 20 $Pr=(c_p*mu)/k;$ // Prandtl number 21 // The constants are assumed as 22 m = 0.8;23 n = 1/3; 24 // Calculation $25 h = C*(k/D_e)*(Re)^m*Pr^n;$ 26 // Result 27 printf(" \n Heat transfer coefficient = %d Btu/hr-ft $^2-F \setminus n$ ",h); 28 // The value is different as compared to the textbook value. This is due to approximation of Reynolds number in the textbook and in this problem actual value is considered.

Scilab code Exa 8.10 Boiling crisis

```
1 // Example 8.10
2 clear all;
3 \text{ clc};
4
5 // Using the data from Example 8.3 to 8.8
6 P = 2000;
                                                 //
     Pressure in psi
7 v = 15.6;
                                                 // Coolant
      velocity in ft/sec
8 D_e = 0.0427;
                                                 //
      Equivalent diameter in ft
9 \, d = 0.42;
                                                 //
     Diameter of the fuel rod in inches
10 b = 0.024;
                                                 //
      Thickness of Zircaloy-4 clad in inches
11 a = (d/2)+b;
                                                 // Radius
      of fuel rods in inches
12 T_b = 600;
                                                 // Bulk
      temeperature in F
13
14 // 1.
15 // Using Bernath correlation
16 // Calculation
17 T_wc = 102.6 * \log(P) - ((97.2*P)/(P+15)) - (0.45*v) + 32;
18 // Result
19 printf(" \n Cladding temperature = \%d F\n", T_wc);
20
21 / / 2.
22 D_i = (2*%pi*a)/(%pi*12);
                                                  // Heated
       perimeter is (2*\%pi*a)/12 in feet
23 // Calculation
24 h_c = 10890*((D_e)/(D_e+D_i))+((48*v)/D_e^0.6);
25 // Result
26 printf(" \n Heat transfer coefficient = %d Btu/hr-ft
      ^2-F \ n",h_c);
27
28 / / 3.
29 // Calculation
```

```
30 q_c = h_c*(T_wc-T_b);
31 // Result
32 printf(" \n Critical heat flux = %.2E Btu/hr-ft^2\n"
,q_c);
33 // In the textbook, the unit of critical heat flux
is wrong.
```

Scilab code Exa 8.11 Engineering sub factor

```
1 // Example 8.11
2 clear all;
3 \, \text{clc};
4
5 // Given data
6 \text{ m_lbar} = 0.457;
                                                // Average
      linear density of UO2 in lb/ft
                                                // Standard
7 \text{ sigma} = 0.0122;
      deviation of set of measured linear densities of
      UO2
8 // Calculation
9 F_Eml = 1+(3*sigma)/m_lbar;
10 printf(" \n Engineering subfactor for the amount of
      fissile material = \%.2 f \setminus n", F_Eml);
```

Scilab code Exa 8.12 Fuel rod calculation

```
1 // Example 8.12
2 clear all;
3 clc;
4
5 q_max = 539000;
    Maximum heat flux Btu/hr-ft^2
```

11

// Hot 6 F = 2.8;channel factor 7 P = 3000;// Reactor thermal power in MW 8 // Expressing in Btu/hr 9 // According to Table 1.9, 1 kW = 3412 Btu/hr 10 $P = P*3.412*10^{6};$ // Reactor thermal power in Btu/hr $11 \ 1 = 12;$ // Length of fuel rod in ft 12 d = 0.5/12; // Diameter of fuel rod in ft 13 r = d/2; 11 Radius of fuel rod in ft 1415 / / 1.16 $q_av = q_max/F$; 17 // Calculation 18 A = P/q_av ; 19 // Result 20 printf(" \n Total heat transfer area = %d ft^2\n",A) ; 2122 / / 2.// The 23 A_one = 2*%pi*r; total surface area of one fuel rod 24 // Calculation $25 n = A/A_one;$ 26 // Result 27 printf(" \n Number of fuel rods = %d \n",n); 28 // The value is different as compared to the textbook value. This is due to approximation of total heat transfer area in the textbook and in this problem actual value is considered. As total heat transfer area is further used to calculate number of fuel rods, therefore the difference in value exists.

Chapter 9

Radiation Protection

Scilab code Exa 9.1 Gamma ray interaction

```
1 // Example 9.1
2 clear all;
3 clc;
4
5 // Given data
6 = 1.6 \times 10^{(-19)};
                                                  11
      Electronic charge in couloumb(coul)
7 X = 1*10^{(-3)}/3600;
                                                  //
      Exposure rate in terms of R/sec
  // According to the definition of Roentgen, 1 R =
8
      2.58*10^{(-7)} coul/g
9 R = 2.58 \times 10^{(-7)};
10 // From standard table
11 // There is 0.001293 g of air per 1 cm<sup>3</sup> at 1
      atmospheric pressure at 0 C
12 density_air = 0.001293;
13 // Calculation
14 IR = (X*R*density_air)/e;
15 // Result
16 printf(" \n Rate of ions produced from gamma ray
      interaction = \%d ions/cm<sup>3</sup>-sec", IR);
```

Scilab code Exa 9.2 Absorbed dose rate and dose equivalent rate

```
1 // Example 9.2
2 clear all;
3 \text{ clc};
4
5 // According to the definition of radiation absorbed
        dose(rad), 1 \operatorname{rad/sec} = 100 \operatorname{ergs/g-sec}
6 // Given data
                                                          11
7 D = 5*10^{(-3)}/100;
      Absorbed dose in terms of rad/sec
  // Expressing absorbed dose rate in SI units
8
9 / / 1 \text{ Gray}(\text{Gy}) = 100 \text{ rad}
10 D_dot = D*3600/100;
11 // Using data from Table 9.2
12 Q = 1;
                                                          //
      Quality factor for gamma rays for tissue
13 // Calculation
14 H_dot = D_dot*Q;
15 printf(' \n Absorbed dose rate in a tissue = \%.1 f
      mGy/hr \setminus n', D_dot*1000);
16 printf(' \n Dose equivalent rate in a tissue = \%.1 f
      mSv/hr \setminus n', H_dot*1000);
```

Scilab code Exa 9.3 Acute radiation exposure

```
1 // Example 9.3
2 clear all;
3 clc;
4
5 // Given data
```

```
6 H = 25;
                                                       11
      Equivalent dose in rem
                                                       // Age
7 \text{ age} = 30;
       of worker in years
8 \exp_age = 77;
                                                       11
      Average age upto which a person lives in years
9 // Using data from Table 9.6
10 // Bone cancer
11 rc_bone = 0.2;
                                                       //
      Risk coefficient per 10<sup>6</sup> rem/year
                                                       //
12 lp_bone = 10;
      Latent period in years
13 // Probability of dying from bone cancer
14 p_bone=(H*rc_bone*(exp_age-(lp_bone+age)))/10^6;
15
16 // Breast cancer
17 \text{ rc_breast} = 1.5;
                                                        //
      Risk coefficient per 10<sup>6</sup> rem/year
18 lp_breast = 15;
                                                        //
      Latent period in years
19 // Probability of dying from breast cancer
20 p_breast = (H*rc_breast*(exp_age-(lp_breast+age)))
      /10^6;
21
22 // Leukemia
23 rc_leukemia = 1;
                                                       11
      Risk coefficient per 10<sup>6</sup> rem/year
24 \text{ lp_leukemia} = 2;
                                                       //
      Latent period in years
25 // Probability of dying from leukemia
26 p_leukemia = (H*rc_leukemia*(exp_age-(lp_leukemia+
      age)))/10^6;
27
28 // Lung cancer
29 \text{ rc_lung} = 1;
                                                       //
      Risk coefficient per 10<sup>6</sup> rem/year
                                                       //
30 \ lp_lung = 15;
      Latent period in years
```

```
31 // Probability of dying from lung cancer
32 p_lung = (H*rc_lung*(exp_age-(lp_lung+age)))/10^6;
33
34 // Pancreatic cancer
35 \text{ rc_pancreas} = 0.2;
                                                       //
      Risk coefficient per 10<sup>6</sup> rem/year
                                                       11
36 lp_pancreas = 15;
      Latent period in years
37 // Probability of dying from Pancreatic cancer
38 p_pancreas = (H*rc_pancreas*(exp_age-(lp_pancreas+
      age)))/10^6;
39
40 // Stomach cancer
41 \text{ rc_stomach} = 0.6;
                                                       //
      Risk coefficient per 10^6 rem/year
42 lp_stomach = 15;
                                                       ||
      Latent period in years
43 // Probability of dying from stomach cancer
44 p_stomach = (H*rc_stomach*(exp_age-(lp_stomach+age))
      )/10^{6};
45
46 // Rest of alimentary cancer
47 \text{ rc}_{ali} = 0.2;
                                                       //
      Risk coefficient per 10<sup>6</sup> rem/year
  lp_ali = 15;
                                                       //
48
      Latent period in years
49
  // Probability of dying from rest of alimentary
      cancer
50 p_ali = (H*rc_ali*(exp_age-(lp_ali+age)))/10^6;
51
52 // Thyroid cancer
53 \text{ rc_thy} = 0.43;
                                                        //
      Risk coefficient per 10<sup>6</sup> rem/year
                                                        11
54 lp_thy = 10;
      Latent period in years
55 // Probability of dying from thyroid cancer
56 p_thy = (H*rc_thy*(exp_age-(lp_thy+age)))/10^6;
57
```

```
58 // All other type of cancer
59 \text{ rc_other} = 1;
                                                       11
      Risk coefficient per 10<sup>6</sup> rem/year
60 lp_other = 15;
                                                       11
      Latent period in years
61 // Probability of dying from all other type of
      cancer
62 p_other = (H*rc_other*(exp_age-(lp_other+age)))
      /10^6;
63
64 // Calculation
65 p = p_bone+p_breast+p_leukemia+p_lung+p_pancreas+
     p_stomach+p_ali+p_thy+p_other;
66 // Result
67 printf('\n Probability that the worker will die from
       cancer = \%.1E \setminus n', p);
68
69 // The value obtained is different from the value
      given in the textbook. This is because of
      approximation of individual probabilities in the
      textbook.
```

Scilab code Exa 9.4 Acute radiation exposure

```
1 // Example 9.4
2 clear all;
3 clc;
4 H = 1; // Equivalent
dos in rem
5 n = 10^6; // Population
6 // Given data
7
8 // Using the data of number of expected deaths of
leukemia per 10^6 people from Table 9.9
9 // In utero age group
```

```
// Fraction of
10 \text{ frac_utero} = 0.011;
      population
11 riskyr_utero = 10;
                                            // Risk years
12 riskcoef_utero = 15;
                                            // Risk
      coefficient
13 // Number of deaths in utero is given by
14 deaths_utero = frac_utero*riskyr_utero*
      riskcoef_utero;
15
16 // In 0-0.99 age group
17 \text{ frac}_0.099 = 0.014;
                                            // Fraction of
      population
18 \text{ riskyr}_0_099 = 25;
                                            // Risk years
19 \text{ riskcoef}_{0.099} = 2;
                                            // Risk
      coefficient
20 // Number of deaths in 0-0.99 age group is given by
21 deaths_0_099 = frac_0_099*riskyr_0_099*
      riskcoef_0_099;
22
23 // In 1-10 age group
24 \text{ frac}_1_10 = 0.146;
                                            // Fraction of
      population
25 \text{ riskyr}_1_{10} = 25;
                                            // Risk years
26 \text{ riskcoef}_{1_{0}} = 2;
                                            // Risk
      coefficient
27 // Number of deaths in 1-10 age group is given by
28 deaths_1_10=frac_1_10*riskyr_1_10*riskcoef_1_10;
29
30 // In 11-20 age group
                                            // Fraction of
31 \text{ frac}_{11}_{20} = 0.196;
      population
32 \text{ riskyr}_{11}_{20} = 25;
                                            // Risk years
33 riskcoef_11_20 = 1;
                                            // Risk
      coefficient
34 // Number of deaths in 11-20 age group is given by
35 deaths_11_20=frac_11_20*riskyr_11_20*riskcoef_11_20;
36
37 // In 21-30 age group
```

```
// Fraction of
38 \text{ frac}_{21}30 = 0.164;
      population
39 \text{ riskyr}_{21}30 = 25;
                                             // Risk years
40 \text{ riskcoef}_{21_{30}} = 1;
                                             // Risk
      coefficient
41 // Number of deaths in 21-30 age group is given by
42 deaths_21_30=frac_21_30*riskyr_21_30*riskcoef_21_30;
43
44 // In 31-40 age group
                                             // Fraction of
45 \text{ frac}_{31}_{40} = 0.118;
      population
46 \text{ riskyr}_{31}_{40} = 25;
                                             // Risk years
47 \text{ riskcoef}_{31}_{40} = 1;
                                                Risk
      coefficient
48 // Number of deaths in 31-40 age group is given by
49 deaths_31_40=frac_31_40*riskyr_31_40*riskcoef_31_40;
50
51 // In 41-50 age group
                                             // Fraction of
52 \text{ frac}_{41}50 = 0.109;
      population
53 \text{ riskyr}_{41}50 = 25;
                                             // Risk years
54 \text{ riskcoef}_{41}50 = 1;
                                             // Risk
      coefficient
55 // Number of deaths in 41-50 age group is given by
56 deaths_41_50 = frac_41_50*riskyr_41_50*
      riskcoef_41_50;
57
58 // In 51-60 age group
                                             // Fraction of
59 \text{ frac}_{51}60 = 0.104;
      population
60 \text{ riskyr}_{51}_{60} = 22.5;
                                             // Risk years
61 \text{ riskcoef}_{51}_{60} = 1;
                                                Risk
                                             11
      coefficient
62 // Number of deaths in 51-50 age group is given by
63 deaths_51_60 = frac_51_60*riskyr_51_60*
      riskcoef_51_60;
64
65 // In 61-70 age group
```

```
66 \ frac_{61}70 = 0.08;
67 \text{ riskyr}_{61}70 = 15.1;
68 \text{ riskcoef}_{61}70 = 1;
                                            // Risk
      coefficient
69 // Number of deaths in 61-70 age group is given by
70 deaths_61_70=frac_61_70*riskyr_61_70*riskcoef_61_70;
71
72 // In 71-80 age group
                                            // Fraction of
73 \text{ frac}_{71}80 = 0.044;
      population
74 \text{ riskyr}_71_80 = 9.1;
                                            // Risk years
                                            // Risk
75 \text{ riskcoef}_{71_80} = 1;
      coefficient
76 // Number of deaths in 71-80 age group is given by
77 deaths_71_80 = frac_71_80*riskyr_71_80*
      riskcoef_71_80;
78
79 // Age greater than 80
80 \text{ frac}_{80} = 0.02;
                                            // Fraction of
      population
81 \text{ riskyr}_80 = 4.5;
                                            // Risk years
82 \text{ riskcoef}_{80} = 1;
                                            // Risk
      coefficient
  // Number of deaths with age greater than 80 years
83
      is given by
84 deaths_80=frac_80*riskyr_80*riskcoef_80;
85
86 // Calculation
87 total_deaths = deaths_utero+deaths_0_099+deaths_1_10
      +deaths_11_20+deaths_21_30+deaths_31_40+
      deaths_41_50+deaths_51_60+deaths_61_70+
      deaths_71_80+deaths_80;
88 // Result
89 printf(" \n Number of cases or deaths expected from
      leukemia = \%.1 f \setminus n", total_deaths);
```

Scilab code Exa 9.5 Chronic radiation exposure

```
1 // Example 9.5
2 clear all;
3 \, \text{clc};
4
5 // Given data
6 \text{ H}_y \text{ear} = 5;
                                                        //
      Equiavelnt dose per year in rem
  start_age = 18;
                                                        //
7
      Initial age of the worker in years
8 \text{ ret}_age = 68;
                                                        //
      Retirement age of the worker in years
  // Using data from Table 9.6 with respect to Bone
9
      cancer
10 latent_period = 10;
                                                        11
      Latent period in years
11 plateau_period = 30;
                                                        //
      Plateau period in years
12 \text{ rc_bone} = 0.2;
                                                        //
      Risk coefficient per 10<sup>6</sup> rem/year
13
14 n = ret_age-(start_age+latent_period);
                                                        //
      Number of years of accumulated dose
15 H = n * H_year;
                                                        //
      Total equivalent dose in rem
16 // Calculation
17 p_bone = (H*rc_bone*plateau_period)/10^6;
18 // Result
19 printf(" \n The probability of dying from bone
      cancer = \%.1E \setminus n", p_bone);
```
Scilab code Exa 9.6 External exposure due to gamma rays

```
1 // Example 9.6
2 clear all;
3 \text{ clc};
4
5 // Given data
6 E = 2;
                                                     //
      Energy of gamma radiation in MeV
  X_dot = 1;
7
                                                      //
      Exposure rate in mR/hour
8 // Using the data from Table II.5
9 // Let mu_a/rho of air at 2 Mev be denoted as mu_rho
10 \text{ mu_rho} = 0.0238;
      Ratio of absorption coefficient to sensity of air
       in cm^2/g
11 // Calculation
12 I = X_dot/(E*mu_rho*0.0659);
13 printf(" \n The beam intensity of gamma radiation
      required = \%d gamma rays/cm<sup>2</sup>-sec \n", ceil(I));
```

Scilab code Exa 9.7 External exposure due to X rays

```
//
10 X_dot_eq = 1;
      Equivalent Exposure rate in mR/hr
11 X_dot = (phi*X_dot_eq)/phi_eq;
                                                    //
      Exposure rate of the operator in mR/hr
12 // From Figure 9.10 at 50 kV energy, the energy
      dependent function is
13 \, \text{f_bone} = 3.3;
14 f_muscle = 0.93;
15 f_fat = 0.9;
16 // Using data from Table 9.2
17 \quad Q = 1;
                                                    //
      Quality factor for x-rays
18 // Calculation
19 D_dot_bone = X_dot*f_bone*Q;
                                                    11
     Dose equivalent rate in bone
20 D_dot_muscle = X_dot*f_muscle*Q;
                                                    //
     Dose equivalent rate in muscle
21 D_dot_fat = X_dot*f_fat*Q;
                                                    11
      Dose equivalent rate in fat
22 // Result
23 printf(" \n Dose equivalent rate in bone = \%d mrem/
     hour \n", ceil(D_dot_bone));
24 printf(" \n Dose equivalent rate in muscle = \%d mrem
      / hour \ \ ceil(D_dot_muscle));
25 printf(" \n Dose equivalent rate in fat = %d mrem/
     hour \n", ceil(D_dot_fat));
```

Scilab code Exa 9.8 External exposure due to neutrons

```
1 // Example 9.8
2 clear all;
3 clc;
4
5 // Given data
6 phi_n = 20;
```

// Given

neutron flux in neutrons/cm²-sec 7 // From Figure 9.128 // To receive an dose equivalent rate of 1 mrem/hr, the fast neutron flux is 7 neutrons/cm²-sec 9 $phi_n = 7;$ 10 $D_dot_eq = 1;$ 11 D_dot_n = (phi_n*D_dot_eq)/phi_n_eq; // Dose rate due to fast neutron flux in mrem/hr // Given 12 phi_th = 300; thermal flux in neutrons/cm²-sec 13 // From Figure 9.12 14 // To receive an dose equivalent rate of 1 mrem/hr, the thermal flux is 260 neutrons/cm²-sec 15 phi_th_eq = 260; 16 D_dot_th = (phi_th*D_dot_eq)/phi_th_eq; // Dose rate due to thermal neutron flux in mrem/hr 17 $D_dot = D_dot_n+D_dot_th;$ // Total dose rate in mrem/hr 18 printf("\n The permitted weekly dose is 100 mrem \n "): 19 D_dot_perm = 100; 20 // Calculation 21 t = D_dot_perm/D_dot; 22 printf(" \n The time of exposure upto a safe level = %.1f hour $\langle n, t \rangle$; 23 // The answer given in the textbook is wrong. This is because of wrong computation of total dose rate

Scilab code Exa 9.9 External exposure due to neutrons

```
1 // Example 9.9
2 clear all;
3 clc;
4
```

```
5 // Given data
6 fluence = 10^8;
                                                      11
      Given fluence neutrons/cm<sup>2</sup>
7 // From Figure 9.12
8 // To receive an dose equivalent rate of 1 mrem/hr,
      the fast neutron flux is 7 neutrons/cm<sup>2</sup>-sec
  phi_eq = 7;
9
                                                     //
      Equivalent flux in neutrons/cm<sup>2</sup>-sec
10 D_eq = 1;
                                                     | |
      Equivalent dose rate in mrem/hr
11 // 1 hour = 3600 seconds
12 fluence_eq = phi_eq*3600;
                                                     //
      Equivalent fluence in neutrons/cm<sup>2</sup>
13 // Calculation
14 D = (fluence*D_eq)/fluence_eq;
15 // Result
16 printf(" \n Dose received due to exposure of
      accelerator source = \%d mrem \n",D);
17 // The answer given in textbook is approximated to a
       nearest value.
```

Scilab code Exa 9.10 Internal exposure due to radionuclide

// Biological 11 $T_12_b = 138;$ half life of Iodine -131 in days 12 lambda = $0.693/T_{12}$; // Radiological decay constant of Iodine-131 in days $^{-1}$ // Biological $13 \ lambda_b = 0.693/T_12_b;$ decay constant of Iodine -131 in days $\hat{-1}$ 14 lambda_e = lambda+lambda_b; // Equivalent decay constant in days -1// Using the data from Table 9.15 15Effective 16 zeta = 0.23;11 energy equivalent in MeV $17 \, q = 0.23;$ // The fraction of Iodine -131 that goes by inhalation 18 // Calculation 19 DCF = (51.1*zeta*q)/(M*lambda_e); 20 // Result 21 printf(" \n The dose commitment factor by inhalation $= \%.2 \, \text{f} \, \text{rem/ucurie} \, \langle n^{"}, \text{DCF} \rangle;$ 2223 // b) 24 breathing_rate = $2.32*10^{(-4)}$; // Normal breathing rate in m^3/sec 25 time = 2*3600;Time of radiation exposure in seconds $I_conc = 2*10^{(-9)};$ // Iodine -131 26concentration 27 CO = breathing_rate*time*I_conc; // Total intake of Iodine -131 by inhalation 28 // Calculation 29 H = $CO*(DCF*10^6)$; // Using DCF in micro-curie 30 // Result 31 printf(" \n The dose commitment to thyroid = %.2Erem = $\%.2 \, f \, \text{mrem} \, \langle n, H, H*1000 \rangle$;

Scilab code Exa 9.11 Maximum Permissible Concentration

```
1 // Example 9.11
2 clear all;
3 \, \text{clc};
4
5 // Given data
6 V_W = 2200;
                                            // Volume of
      water inatke in terms of cm^3/day
7 // 1 litre = 1000 \text{ gram}(g)
                                            // Mass of
8 M = 43 * 1000;
      water present in standard man according to
      standards
9 // Using the data from Table 9.13
10 MPD = 0.1/7;
                                            // Maximum
      Permissible Dose (MPD) in rem/day
11 // Using the data from Table 9.15
12 zeta = 0.01;
                                               Effective
                                            11
      energy equivalent in MeV
                                            // The
13 \, q = 1;
      fraction of Tritium that goes inside by ingestion
14 T_b = 11.9;
                                            // Biological
      Half life of Tritium in years
                                            // Biological
  lambda_b = 0.693/T_b;
15
      decay constant of Tritium in years<sup>-1</sup>
16
17 // As biological and radiological half lives are
      less than 50 year intake period, the exponential
      term (\exp(-\text{lambda}_e * 50)) is neglected
18 // Maximum Permissible Concentration (MPC) for a 7
      day or 168 hour week tritium dose
19 MPC_w_168 = (lambda_b*M*MPD)/(51.1*V_W*zeta*q);
20 printf("\n Maximum Permissible Concentration(MPC)
      for a 7 day or 168 hour week tritium dose for
```

occupational purpose = $\%.2 \text{ f uCi/cm^3} \n"$, MPC_w_168); 21 // The exposure at work is doubled for 40 hour week as compared to 168 hour week 22 // For 40 hour week, with work of 5 days out of 7 day week according to a study $23 \text{ MPC}_w_40 = \text{MPC}_w_168 * 2 * (7/5);$ 24 **printf**("\n Maximum Permissible Concentration(MPC) for a 40 hour week tritium dose for occupational purpose = $\%.3 f uCi/cm^3 \langle n^{"}, MPC_w_40 \rangle$; 2526 // By analyzing the data of Table 9.13 27 // The whole body dose of general public is one tenth of the occupational purpose. $28 \text{ MPC}_w_{168}\text{gp} = \text{MPC}_w_{168*0.1};$ 29 **printf**("\n Maximum Permissible Concentration(MPC) for a 7 day or 168 hour week tritium dose for general public = %.3 f uCi/cm³ \n", MPC_w_168_gp); 30 // The answer of Maximum Permissible Concentration (MPC) for a 168 hour week tritium dose for general public is given wrong in the textbook.

Scilab code Exa 9.12 Acute radiation exposure

```
1 // Example 9.12
2 clear all;
3 clc;
4 
5 // Given data
6 no_home = 10^6; //
Number of houses
7 no_resident = 4; //
Number of residents in a home
8 total_time = 50; //
Number of years the analysis is carried out
```

```
9 radon_concn_old = 1;
                                                    11
     Radon concentration in older uninsulated homes in
       terms of pCi/l
10 radon_concn_new = 6;
                                                    11
     Radon concentration in modern insulated homes in
      terms of pCi/l
11 time = 3500;
                                                    11
     Time spent in home by a person per year in hours
12 eq_concn = 0.5;
                                                    //
      Equilibrium concentration of 50%
13 // 1 \text{ year} = 24*365 \text{ hours}
14 X_increased = eq_concn*(radon_concn_new-
     radon_concn_old)*(time/(24*365));
                                          // The
      increased exposure of radon per person
15
16 // Using the data of Radon risk assessment of United
       States of America
17 // There are nearly 100 cases of cancer per 10^{6}
      persons at 1 pCi-year dose.
18 // Calculation
19 no_cancer = (no_home*no_resident)*total_time
      *(100/10<sup>6</sup>)*X_increased;
20 // Result
21 printf("\n Number of additional cases of cancer from
       insulation of home = \%d \n",no_cancer);
22 // There is a slight deviation in the value given in
      the textbook. This is because of approximation
      of the number of additional cases of cancer in
      the textbook.
```

Scilab code Exa 9.13 Acute radiation exposure

```
1 // Example 9.13
2 clear all;
3 clc;
```

```
4
5 // Given data
                                                       11
6 \text{ H_ext} = 3;
      External dose in rem
7 \text{ H_wbL} = 5;
                                                       11
      Annual whole body dose limit in rem
8 // Using the data from Table 9.17
9 // Annual Limit Intake (ALI) for inhalation of
      Iodine -131 is 54 uCurie (Ci)
10 ALI = 54;
11 // Calculation
12 I = ALI*(1-(H_ext/H_wbL));
13 // Result
14 printf("\n Amount of Iodine -131 intake within safety
       limits = \%d uCi \langle n, ceil(I) \rangle;
```

Chapter 10

Radiation Shielding

Scilab code Exa 10.1 Gamma ray buildup factor

```
1 // Example 10.1
2 clear all;
3 \, \text{clc};
4
5 // Given data
                                                           //
6 E0 = 2;
      Energy of gamma rays in MeV
7 a = 10;
                                                          //
      Thickeness of lead shield in cm
8 \text{ phi0} = 10^{6};
                                                          11
      Intensity of gamma rays in gamma-rays/cm<sup>2</sup>-sec
9
10 // 1.
11 // Using the data from Table II.4 for \rm E0 = 2 MeV
                                                          // The
12 \text{ mu_rho} = 0.0457;
       ratio of total attenuation coefficient to
      density in cm^2/g
13 // From standard data tables for lead
                                                          11
14 \text{ rho} = 11.34;
      Density of lead in g/cm<sup>3</sup>
15 // Calculation
```

```
16 phi_u = phi0*exp(-(mu_rho*rho*a));
17 // Result
18 printf("\n Uncollided flux at the rear side of lead
      shield = \%.2E gamma-rays/cm<sup>2</sup>-sec \n",phi_u)
19
20 / / 2.
21 // Using the data from Table 10.1 for 2 MeV of lead
      material
22 mua = mu_rho*rho*a;
                                                       11
23 \quad B_4 = 2.41;
      Buildup factor if mu*a = 4
24 B_7 = 3.36;
                                                       11
      Buildup factor if mu*a = 7
25 // Using two point method of straight line for
      calculating buildup factor at mu*a
26 B_m = B_4 + ((mua-4) * ((B_7-B_4)/(7-4)));
27 // Calculation
28 phi_b = phi_u*B_m;
29 // Result
30 printf("\n Buildup flux at the rear side of lead
      shield = \%.2E gamma-rays/cm<sup>2</sup>-sec \n", phi_b);
31
32 // 3.
33 // Using the data from Table II.5 for 2 MeV
34 mua_rho_air = 0.0238;
                                                       11
      The ratio of total attenuation coefficient to
      density of air in cm^2/g
35 // Calculation
36 X_dot = 0.0659*E0*mua_rho_air*phi_b;
37 // Result
38 printf("\n Exposure rate at the rear side of lead
      shield = \%.1 f mR/hour \n", X_dot);
```



Figure 10.1: Gamma ray buildup factor

Scilab code Exa 10.2 Gamma ray buildup factor

```
1 // Example 10.2
2 clear all;
3 \, \text{clc};
4
5 // Given data
                                                        //
6 E = 1;
      Energy of gamma rays in MeV
  X_dot = 1;
                                                        //
7
      Exposure rate in mR/hour
8 \text{ phi0} = 10^8;
                                                        11
      Intensity of gamma rays in gamma-rays/cm<sup>2</sup>-sec
      from isotropic point source
9 // Using the data from Table II.5 for 1 MeV
10 mua_rho_air = 0.028;
                                                          //
      The ratio of total attenuation coefficient to
      density of air in cm^2/g
11 phi_b = X_dot/(0.0659*E*mua_rho_air);
                                                       //
      Buildup flux in gamma-rays/cm<sup>2</sup>-sec
12 // Using Eq 10.14
13 printf(" \n The equation to calculate radius is \ln \%
      .2E = \%E * Bp*exp(-mu*R) / (4*pi*R^2) \ \n",phi_b,
      phi0);
14 // Using the data from Table II.4 for E = 1 MeV for
      Iron
                                                      // The
15 \text{ mu_rho} = 0.0595;
       ratio of total attenuation coefficient to
      density in cm^2/g
16 // From standard data tables for iron
                                                      //
17 \text{ rho} = 7.864;
      Density of iron in g/cm<sup>3</sup>
18 mu = mu_rho*rho;
19 // On solving the right hand side of equation
20 // RHS = 3.22*10^{3}*Bp*exp(-mu*R)/(mu*R)^{2}
21 // Let mu * R = x
22 // Using the data from Table 10.2 for isotropic
      point source of 1 MeV incident on iron material
```

```
23 Bp = [1.87 \ 2.89 \ 5.39 \ 10.2 \ 16.2 \ 28.3 \ 42.7];
24 x = [1 2 4 7 10 15 20];
25 \text{ for } i = 1:7
       RHS(i) = (3.22*10^3*Bp(i)*exp(-x(i))/x(i)^2);
26
27 end
28 plot2d("nl",x(:),RHS(:));
29 xlabel("mu * R");
30 ylabel("RHS");
31 title("Semilog plot of RHS vs mu*R")
32 // From the graph
33 \text{ muR} = 6.55;
                                                       //
      This is the value when RHS = 1
34 // Calculation
35 R = muR/mu;
36 // Result
37 printf("\n The shield radius required = \%d cm \n",
      ceil(R));
```

Scilab code Exa 10.3 Shielding of infinite planar source

```
1 // Example 10.3
2 clear all;
3 \, \text{clc};
4
5 // Given data
6 = 2;
                                                         11
     Energy of gamma rays in MeV
                                                         11
7 X_dot = 2.5;
     Exposure rate in mR/hour
8 \text{ phi0} = 10^9;
                                                         //
     Intensity of gamma rays in gamma-rays/cm<sup>2</sup>-sec
     from isotropic point source
9 // Using the data from Table II.5 for 1 MeV
```



Figure 10.2: Shielding of infinite planar source

```
10 mua_rho_air = 0.0238;
                                                            //
      The ratio of total attenuation coefficient to
      density of air in cm^2/g
11 phi_b = X_dot/(0.0659*E*mua_rho_air);
                                                           //
      Buildup flux in gamma-rays/cm<sup>2</sup>-sec
12
13 // From standard data tables for concrete
14 rho = 2.35;
                                                            11
      Density of concrete in g/cm^3
  // Using the data from Table 10.3 for concrete at 2
15
      MeV
16 \quad A1 = 18.089;
17 \quad A2 = 1 - A1;
18 \text{ alpha1} = -0.0425;
19 \text{ alpha2} = 0.00849;
20 // Using Eq 10.26
21 printf(" \n The equation to calculate thickness is \setminus
      n \%.2E = (\%E/2) * (\%4.3 \text{ f} *E1(\%4.3 \text{ f} *mu*a) \%4.3 \text{ f} *E1(
      \%4.3 \text{ f} * \text{mu} * \text{a})) \ \ n", phi_b, phi0, A1, (1+alpha1), A2, (1+
      alpha2));
22 // Using the data from Table II.4 for E = 1 MeV for
      concrete
                                                         // The
23 \text{ mu_rho} = 0.0445;
       ratio of total attenuation coefficient to
      density in cm^2/g
24 mu = mu_rho*rho;
25 // On solving the right hand side of equation
  // RHS = 1.13*10^7*(E1(0.9575*mu*a) -0.94*E1(1.00849*
26
      mu*a))
27 // Let mu*a = x
28 x = 1:20
29 \text{ for } i = 1:20
        RHS(i) = 1.13*10^7*(exp(-0.9575*x(i)))
30
           *((1/(0.9575*x(i))+(1/(0.9575*x(i))^3))) -
           exp(-1.00849 * x(i)) * ((1/(1.00849 * x(i)))
           +(1/(1.00849*x(i))^3)));
31 end
32 plot2d("nl",x(:),RHS(:));
```

```
33 xlabel("mu*a");
34 ylabel("RHS");
35 title("Semilog plot of RHS vs mu*a")
36 // From the graph
37 mua = 13.6; //
This is the value when RHS = 1
38 // Calculation
39 a = mua/mu;
40 // Result
41 printf("\n The concrete thickness = %d cm \n",a);
```

Scilab code Exa 10.4 Multilayered shielding

1 // Example 10.4 2 clear all; 3 clc;4 5 // Given data 6 E = 6;// Energy of gamma rays in MeV $7 \text{ phi0} = 10^2;$ 11 Intensity of gamma rays in gamma-rays/cm²-sec from mono-directional beam $8 x_w = 100;$ // Thickness of water in cm $9 x_Pb = 8;$ 11 Thickness of lead in cm 10 // Using data from Table II.4 at 6 MeV 11 $mu_w = 0.0275;$ Total attenuation coefficient of water in $cm^{(-1)}$ $12 \text{ mu}_{Pb} = 0.4944;$ Total attenuation coefficient of lead in $\operatorname{cm}^{-}(-1)$ 13// 14 $mua_w = x_w*mu_w;$ Attenuation due to thickness of water

```
//
15 mua_Pb = x_Pb*mu_Pb;
      Attenuation due to thickness of lead
16
17 // Case (a) - Water is placed before the lead
18 printf(" \n In case (a), Buildup factor is only due
      to lead measured at %.2f",mua_Pb);
19 // Using the data from Table 10.1 at 6 MeV
20 B_Pb = 1.86;
21 phi_b_a = phi0*B_Pb*exp(-(mua_w+mua_Pb));
22
23 // Using the data from Table II.5 for 6 MeV
24 \text{ mua_rho_air} = 0.0172;
                                                       11
      The ratio of total attenuation coefficient to
      density of air in cm^2/g
25 // Calculation
26 X_dot_a = 0.0659*E*mua_rho_air*phi_b_a;
27 // Result
28 printf("\n Exposure rate if water is placed before
      lead shield = \%.2 \, \text{f uR/hour } n", X_dot_a*1000);
29
30 // Case (b) - Lead is placed before water
31 printf(" \n In case (b), Buildup factor is due to
      water and lead measured at %.2f and %.2f
      respectively", mua_w, mua_Pb);
32 // Using the data from Table 10.1 for water at 3.2
     MeV,, which is the minimum point of mu_Pb curve
33 \quad B_w = 2.72;
34 \quad B_m = B_Pb * B_w;
35 phi_b_b = phi0*B_m*exp(-(mua_w+mua_Pb));
36
37 // Calculation
38 X_dot_b = 0.0659*E*mua_rho_air*phi_b_b;
39 // Result
40 printf("\n Exposure rate if lead is placed before
      water = \%.2 \text{ f uR/hour } \text{n}", X_dot_b*1000);
41 // The answer given in the textbook is wrong. This
      is because the intensity of gamma rays is wrongly
       taken for calculation.
```

Scilab code Exa 10.5 Removal cross section

```
1 // Example 10.5
2 clear all;
3 \text{ clc};
4
5 // Given data
6 fission_density = 4*10^7;
                                                         //
      Fission density in fissions/cm<sup>2</sup>-sec
7 / / 1 inches = 2.54 cm
8 d = 28 * 2.54;
                                                         //
      Diamaeter of plate in cm
9 R = d/2;
                                                         //
      Radius of plate in cm
10 v = 2.42;
                                                         11
      Number of fission neutrons emitted per fission
11 x = 75;
                                                         //
      Distance of point from center of plate in cm
12 // Using the data from Table 10.4 for removal
      macroscopic cross section of water
13 \text{ sigma_RW} = 0.103;
      Removal macroscopic cross section of water in cm
      ^{-1}
14 S = v*fission_density;
                                                         11
      Strength of neutron source in terms of neutrons/
      \mathrm{cm}^2 - \mathrm{sec}
15 \quad A = 0.12;
                                                         // A
       constant
16 // From Figure 10.19
17 tan_theta = R/x;
18 theta = atan(R/x);
19 sec_theta = sec(theta);
20
21 // 1.
```

```
//
22 \times 11 = sigma_RW * x;
      Exponential integral function
                                                      11
23 x21 = sigma_RW*x*sec_theta;
      Exponential integral function
24 // Let the upper limit of integral be 20
25 x_1imit = 20;
26 function y=f(x), y=exp(-x)/x, endfunction
27 E1_x11 = intg(x11,x_limit,f);
    E1_x21 = intg(x21, x_limit, f);
28
29 // Calculation
30 phi_1 = S*A/2*(E1_x11-E1_x21);
31 // Result
32 printf(" \n The fast flux without iron shield = \%d
      neutrons/cm<sup>2</sup>-sec n", phi_1);
33
34 // 2. Iron slab is inserted in front of the fission
      plate
35 // Using the data from Table 10.4 for removal
      macroscopic cross section of iron
36 \text{ sigma}_R = 0.168;
                                                      11
      Removal macroscopic cross section of iron in cm
      ^{-1}
37 t = 3*2.54;
                                                      11
      Thickness of iron slab in cm
  // Now the analysis is similar to multi layered
38
      shielding
39 x12 = sigma_RW*x+sigma_R*t;
                                                       //
      Exponential integral function
40 x22 = sigma_RW*x*sec_theta+sigma_R*t*sec_theta; //
      Exponential integral function
41 // Let the upper limit of integral be 20
42 \text{ x_limit} = 20;
43 function y=f(x),y=exp(-x)/x,endfunction
44 E1_x12 = intg(x12, x_limit, f);
45
    E1_x22 = intg(x22,x_limit,f);
46 // Calculation
47 phi_2 = S*A/2*(E1_x12-E1_x22);
48 // Result
```

49 printf(" \n The fast flux with iron shield = %.1f neutrons/cm²-sec \n",phi_2);

Scilab code Exa 10.6 Removal cross section

1 // Example 10.6 2 clear all; $3 \, \text{clc};$ 4 5 // Given data 6 // Assuming average energy produced per fission reaction is 200 MeV $7 P = 250 * 10^3$: 11 Power of research reactor in Watts 8 P_fission = 200*10^6*1.6*10^(-19); 11 Energy produced in a fission reaction in terms of joule 9 f = 0.75;Metal volume fraction 10 // In this problem, both reflector and shield act as a composite shield 11 a = 150+15; // Net shield distance in cm 12 // 1 litre = 1000 grams 13 V = 32*1000; 11 Core volume in gram 1415 fission_density = (P/P_fission)*(1/V); 16 v = 2.42;11 Number of fission neutrons emitted per fission 17 S = fission_density*v; // Neutron source strength in neutrons/cm³-sec 18 // Assuming spherical shape 19 // Volume of sphere = $(4/3) * pi * (radius)^3$ 20 R = $((3*V)/(4*\%pi))^{(1/3)};$

21	// Using the data from Table 10.4 for removal
	macroscopic cross section
22	sigma_R = 0.174; //
	Removal macroscopic cross section of uranium in
22	$\operatorname{CIII} - \mathbf{I}$
23	sigma_RW = 0.103; //
	Removal macroscopic cross section of water in cm
	^ -1
24	A = 0.12; // A
	constant
25	alpha = ((1-f)*sigma_RW)+(f*sigma_R); // A
	parameter
26	// Calculation
27	theta = $(S*A/(4*alpha))*(ceil(R)/(ceil(R)+a))^2*exp$
	(-sigma RW*a)*(1-exp(-2*alpha*ceil(R))):
28	// Converting into equivalent dose rate by referring
20	Figure 0.12
20	// East neutron flux of 6.8 neutrons/ m^2 see is
29	// Fast neutron flux of 0.8 neutrons/cm 2-sec is
	equivalent to 1 mrem/hr
30	H_dot = theta/6.8;
31	// Result
32	printf(" \n Fast neutron dose rate near the surface
	of the shield = $\%.1$ f mrem/hour \ln ", H_dot);

Scilab code Exa 10.7 Dose equivalent rate and thickness

```
1 // Example 10.7
2 clear all;
3 clc;
4 
5 // Given data
6 E = 14; //
Energy of neutrons in MeV
7 phi0 = 10^9; //
Intensity of neutrons in neutrons/cm<sup>2</sup>-sec from
```

isotropic point source 8 / / 1 feet = 30.48 cm $9 \, d = 10 * 30.48;$ Distance of concrete wall from a point source in cm 10 // As Intensity obeys inverse square law 11 I = phi0/(4*%pi*d^2); 11 Intensity of neutron beam in terms of neutrons/cm $^2 - \sec$ 12 $H_dot = 1;$ 11 The required dose equivalent rate in mrem/hour 13 // From Figure 10.23(b) 14 HO_dot = H_dot/I ; // The dose equivalent rate 15 // Result 16 printf(" \n The reduced dose equivalent rate due to concrete wall is $= \%.2E \text{ mrem/hr } \text{n",HO_dot}$; 17 // By looking into Figure 10.23(b) on thickness axis 18 printf(" \n The concrete slab thickness is = 70 cm \ n");

Scilab code Exa 10.8 Shielding of prompt fission gamma rays

```
1 // Example 10.8
2 clear all;
3 clc;
4
5 // Given data
6 R = 7*30.48; //
Distance of core from the center of shield in cm
7 // Assuming average energy produced per fission
reaction is 200 MeV
8 P = 10; //
Power of teaching reactor in Watts
9 P_fission = 200*10^6*1.6*10^(-19); //
```

Energy produced in a fission reaction in terms of joule 10 fission_rate = P/P_fission; // Number of fission reactions 11 12 // By assuming that the gamma rays are of equal energy of 1 MeV (Group 1) and looking into Table 10.513 E1 = 1; // Energy of gamma rays in MeV (Assumed) $14 \text{ chi}_{pn1} = 5.2;$ Number of prompt gamma rays emitted per fission with energy 2 MeV 15 S1 = chi_pn1*fission_rate; // Source strength in gamma rays/sec // Using the data from Table II.4 for E = 1 MeV for 16water 17 mu1 = 0.0996;11 Mass attenuation coefficient at 1 MeV in cm^{-1} 18 printf(" \n Buildup factor is due to water measured at %.2 f",mu1*R); 19 // Using the data from Table 10.2 at 1 MeV $20 \quad B_p1 = 373;$ 21 phi_b1 = (S1/(4*%pi*R^2))*B_p1*exp(-mu1*R); 11 Buildup flux 22 // Using the data from Table II.5 for 1 MeV $23 \text{ mua_rho_air1} = 0.028;$ | | The ratio of total attenuation coefficient to density of air in cm^2/g 24 // Calculation 25 X_dot1 = 0.0659*E1*mua_rho_air1*phi_b1; 26 printf("\n Exposure rate due to group 1 = %.4 f mR/ hour $\langle n^{"}, X_{dot1} \rangle$; 2728 // By assuming that the gamma rays are of equal energy of 2 MeV (Group 2) and looking into Table 10.529 E2 = 2;//

Energy of gamma rays in MeV (Assumed) 30 chi_pn2 = 1.8; 11 Number of prompt gamma rays emitted per fission with energy 2 MeV 31 S2 = chi_pn2*fission_rate; // Source strength in gamma rays/sec 32 // Using the data from Table II.4 for E = 2 MeV for water 33 mu2 = 0.0493;11 Mass attenuation coefficient at 2 MeV in cm^{-1} 34 printf(" \n Buildup factor is due to water measured at %.2 f",mu2*R); 35 // Using the data from Table 10.2 at 2 MeV $36 B_p2 = 13.1;$ 37 phi_b2 = (S2/(4*%pi*R^2))*B_p2*exp(-mu2*R); 11 Buildup flux 38 // Using the data from Table II.5 for 2 MeV 39 mua_rho_air2 = 0.0238; 11 The ratio of total attenuation coefficient to density of air in cm^2/g 40 // Calculation 41 X_dot2 = 0.0659*E2*mua_rho_air2*phi_b2; 42 printf("\n Exposure rate due to group $2 = \%.1 \,\mathrm{f} \,\mathrm{mR}/$ hour $\n", X_dot2);$ 4344 // By assuming that the gamma rays are of equal energy of 4 MeV (Group 3) and looking into Table 10.545 E3 = 4;11 Energy of gamma rays in MeV (Assumed) $46 \text{ chi}_pn3 = 0.22;$ 11 Number of prompt gamma rays emitted per fission with energy 4 MeV 47 S3 = chi_pn3*fission_rate; 11 Source strength in gamma rays/sec 48 // Using the data from Table II.4 for E = 4 MeV for water 49 mu3 = 0.0339;//

Mass attenuation coefficient at 4 MeV in cm^{-1} 50 printf(" \n Buildup factor is due to water measured at %.1f",mu3*R); 51 // Using the data from Table 10.2 at 4 MeV $52 B_p3 = 5.27;$ 53 phi_b3 = (S3/(4*%pi*R^2))*B_p3*exp(-mu3*R); // Buildup flux 54 // Using the data from Table II.5 for 4 MeV 55 mua_rho_air3=0.0194; // The ratio of total attenuation coefficient to density of air in cm^2/g 56 // Calculation 57 X_dot3 = 0.0659*E3*mua_rho_air3*phi_b3; 58 printf("\n Exposure rate due to group 3 = %.1 f mR/ hour $\langle n^{"}, X_{dot3} \rangle$; 5960 // By assuming that the gamma rays are of equal energy of 6 MeV (Group 4) and looking into Table 10.5 $61 \quad E4 = 6;$ // Energy of gamma rays in MeV (Assumed) $62 \text{ chi}_pn4 = 0.025;$ 11 Number of prompt gamma rays emitted per fission with energy 4 MeV 63 S4 = chi_pn4*fission_rate; 11 Source strength in gamma rays/sec 64 // Using the data from Table II.4 for E = 6 MeV for water 65 mu4 = 0.0275;11 Mass attenuation coefficient at 6 MeV in cm^{-1} 66 printf(" \n Buildup factor is due to water measured at %.2 f",mu4*R); 67 // Using the data from Table 10.2 at 6 MeV $68 \quad B_p4 = 3.53;$ 69 phi_b4 = (S4/(4*%pi*R^2))*B_p4*exp(-mu4*R); // Buildup flux 70 // Using the data from Table II.5 for 4 MeV 71 mua_rho_air4=0.0172; //

```
The ratio of total attenuation coefficient to
    density of air in cm<sup>2</sup>/g
72 // Calculation
73 X_dot4 = 0.0659*E4*mua_rho_air4*phi_b4;
74 printf("\n Exposure rate due to group 3 = %.2f mR/
    hour \n",X_dot4);
75
76 //Calculation
77 X_dot = X_dot1+X_dot2+X_dot3+X_dot4;
78 // Result
79 printf("\n The total exposure rate due to all groups
    = %.2f mR/hour \n",X_dot);
```

Scilab code Exa 10.9 Coolant activity

```
1 // Example 10.9
2 clear all;
3 \text{ clc};
4
5 // Given data
6 // Assuming average energy produced per fission
      reaction is 200 MeV
7 P = 55;
                                                            //
      Power density of reactor in watts/cm<sup>3</sup>
8 \text{ rho}_{eff}U = 0.33;
                                                            //
      Effective density of uranium in g/cm<sup>3</sup>
9 rho_eff_W = 1-rho_eff_U;
                                                            //
      Effective density of water in g/cm<sup>3</sup>
10 t_i = 3;
                                                            11
      Average time spent by water in the reactor in
      seconds
11 t_0 = 2;
                                                            //
      Average time spent by water in the external
      coolant circuit in seconds
12 / / 1 \text{ eV} = 1.6 * 10^{(-19)} \text{ J}
```

13 $P_{fission} = 200*10^{6}*1.6*10^{(-19)};$ 11 Energy produced in a fission reaction in terms of joule 14 fission_density = P/P_fission; // Number of fission reactions 15 v = 2.42; 11 Number of fission neutrons emitted per fission 16 S = v*fission_density; 11 Strength of neutron source in terms of neutrons/ $\mathrm{cm}^2 - \mathrm{sec}$ 17 // Atom density of oxygen at normal density of 1 g/ cm³ is 18 rho = 1;// Density of water in g/cm^3 19 $N_A = 6.02 \times 10^{(23)};$ 11 Avogadro's constant 20 M = 18;11 Molecular weight of water 21 atom_density = (rho*N_A)/M; 2223 // Using the data from Table 10.7 $24 \text{ sigma_r} = 1.9*10^{(-5)}*10^{(-24)};$ // Reaction cross section in cm² $T_{12} = 7.1;$ 25// Half life of the given reaction in seconds 26 $lambda = 0.693/T_{12};$ // Decay constant of the given reaction in seconds (-1)27 sigma_act = rho_eff_W*atom_density*sigma_r; // Average macroscopic activation cross section 28 // Using the data from Table 10.4 $29 \text{ sigma_RW} = 0.103;$ // Removal cross section of water in cm^{-1} $30 \text{ sigma_RU} = 0.174;$ 11 Removal cross section of Uranium in cm^{-1} 31 sigma_R = (sigma_RU*rho_eff_U)+(sigma_RW*rho_eff_W); // Removal cross section of mixture 32 // Let activation rate given by (sigma_act*phi_av)

```
be denoted as AR
33 AR = (sigma_act*S)/sigma_R;
34 // Calculation
35 alpha = AR*(1-exp(-t_i*lambda))/(1-exp(-(t_i+t_0)*
lambda));
36 // 1 curie = 3.7*10^(10) disintegrations/sec
37 // Result
38 printf("\n Equilibrium activity of water due to
neutron capture of oxygen = %.2E disintegrations/
cm^3-sec or %d uCi/cm^3 \n",alpha,ceil(alpha
*10^6/(3.7*10^10)));
```

Chapter 11

Reactor Licensing Safety and the Environment

Scilab code Exa 11.1 Diffusion of radioactive effluents

```
1 // Example 11.1
2 clear all;
3 \text{ clc};
4
5 // Given data
6 h = 30;
                                                 //
     Height at which the effluent is relaesed
7 // Calculation of maxima location
8 sigma_z = h/sqrt(2);
                                                 //
      Vertical dispersion coefficient
9 // Using the plot given in Figure 11.12 for Type F
     condition
10 // The corresponding value with calculated maximum
     location is noted.
11 h_max = 1900;
12 // Result
13 printf(" \n The point of maximum concentration of
     non-radioactive effluent = \%d m \n", h_max);
```

Scilab code Exa 11.2 External dose from gamma rays

```
1 // Example 11.2
2 clear all;
3 \, \text{clc};
4
5 // Given data
6 \quad A = 2 * 10^3;
                                                   11
      Amount of radioactivity release due to Xenon-133
      in curie
                                                   // Time
7 t = 365 * 24 * 3600;
      in seconds
8 Q_dash = A/t;
                                                   //
      Average emission rate of Xenon-133
9 h = 100;
                                                   //
      Location of radioactivity release through vent
10 v_bar = 1;
                                                   // Wind
      speed in m/sec
11 // Using the plot given in Figure 11.11 and 11.12
      for Type F condition at 100 m
12 \text{ sigma_y} = 275;
                                                   //
      Horizontal dispersion coefficient
13 sigma_z = 46;
                                                   //
      Vertical dispersion coefficient
14 chi = (Q_dash*exp(-h^2/(2*sigma_z^2)))/(%pi*v_bar*
      sigma_y*sigma_z);
                          // Radionuclide
      concentration in terms of Ci/cm<sup>3</sup>
15 // Using data from Table 11.3
16 \text{ Eg_bar} = 0.03;
      Average gamma decay energy per disintegration in
      MeV
17 // Calculation
18 H_dot = 0.262*chi*Eg_bar*t*10^3;
                                                   // The
      units are in mrem/year
```

```
19 // Expressing the dose rate in SI units
20 H_dot_SI = 2.62*chi*Eg_bar*t*10^3;
21 // Result
22 printf(" \n The external gamma dose rate due to
        xenon release under type F condition = %.4 f mrem/
        year or %.3 f mSv/year \n",H_dot,H_dot_SI);
```

Scilab code Exa 11.3 External dose from gamma rays

```
1 // Example 11.3
2 clear all;
3 clc;
4
5 // Using data from Table 11.3
6 Eg_bar = 0.00211; //
Average gamma decay energy per disintegration in
MeV
7 // Calculation
8 C_y = 0.262*Eg_bar;
9 // Result
10 printf(" \n The dose rate factor due to krypton
exposure = %.2E rem*m^3/sec-Ci \n",C_y);
```

Scilab code Exa 11.4 External dose from gamma rays

```
7 t = 365 * 24 * 3600;
                                                         //
      Time in seconds
8 // Using data from Table 11.3
9 Ebeta_bar = 0.146;
                                                         11
      Average gamma decay energy per disintegration in
      MeV
10 f = 1;
                                                         11
      Experimentally detemined factor
11 // Calculation
12 H_dot = 0.229*Ebeta_bar*chi*f*t;
13 // Expressing the result in milli-rem
14 printf(" \n The external beta dose rate due to xenon
       exposure for a year = \%.3 \, \text{f} \, \text{mrem/year} \, \text{n}", H_dot
      *10^3);
```

Scilab code Exa 11.5 Dose rate to thyroid

1 // Example 11.5 2 clear all; 3 **clc**; 4 5 // Given data $6 \quad A = 1.23;$ 11 Amount of radioactivity release due to I-131 in curie in one year 7 h = 30;11 Location of radioactivity release through vent in meter $8 v_bar = 1.2;$ // Wind speed in m/sec // Half $9 T_{12} = 8.04;$ life of Iodine 131 in days $10 T_{12b} = 138;$ 11 Biological half life of Iodine 131 in days 11 zeta = 0.23; //

Fraction of core inventory in MeV 12 q = 0.23;11 Fraction of Iodine -131 in thyroid 13 M = 20; // Mass of an adult thyroid in grams 1415 // 1. 16 t = 365 * 24 * 3600;// Time in seconds 17 Q_dash = A/t; // Average emission rate of Iodine-131 18 // Converting days into seconds by using 1 day = 86400 seconds 19 lambda = $0.693/(T_{12}*86400);$ // Decay constant of Iodine -131 $lambda_b = 0.693/(T_12b*86400);$ 20// Biological decay constant of Iodine -131 21 // Let the quantity $chi*v_bar/Q_bar = x$ 22 // Using the plot given in Figure 11.13 for Type E condition at 2000 m $23 x = 6*10^{(-5)};$ 24 // Solving for chi 25 chi = $(x*Q_dash)/v_bar;$ 26 // As per the standards of International Commission on Radiolgical Protection (ICRP) $27 B = 2.32*10^{(-4)};$ // Normal breathing rate in m^3/sec 28 // Calculation 29 H_dot = (592*B*zeta*q*chi)/(M*(lambda+lambda_b)); 30 // Result 31 printf(" \n The equilibrium dose rate to an adult thyroid = %.2E rem/sec \n", H_dot); 3233 / / 2.34 // Calculation $35 \text{ H} = \text{H}_{\text{dot}*t};$ 36 // Expressing the result in milli-rem 37 // Result

38 printf(" \n The annual dose to an adult thyroid = % .2 f mrem n",H*10^3);

Scilab code Exa 11.6 Ground exposure from gamma rays

1 // Example 11.6 2 clear all; $3 \, \text{clc};$ 4 5 // Given data 6 E = 0.66;Energy of gamma ray emitted by caesium in MeV 7 x = 100;11 Height of exposure in cm 8 // Using the data from Table II.5 for air at E =0.66 MeV $9 \text{ mua_rho} = 0.0294;$ // The ratio of absorption coefficient to density of air in cm^2/g 10 // Using the data from Table II.4 for air at E =0.66 MeV 11 $mu_rho = 0.0775;$ 11 The ratio of attenuation coefficient to density of air in cm^2/g 12 // Using standard value for density of air 13 rho = $1.293 \times 10^{(-3)}$; 14 mu = mu_rho*rho; 15 mux = mu*x; 16 gamma = 0.57722;// Euler's constant 17 E1 = -gamma + log(1/mux) + mux;// Conversion factor 18 // Using parameter data from Table 11.16 19 C = 1.41;// A constant

Scilab code Exa 11.7 External dose from gamma rays

1 // Example 11.7 2 clear all; 3 clc;4 5 // Given data $6 \quad CO = 6.25 * 10^{6};$ Amount of initial radioactivity release due to I -131 in curie 7 p = 0.1;11 Leakage rate in percent 8 t0 = 2*3600;// Analysis time in seconds $9 v_bar = 1;$ // Wind speed in m/sec 10 11 // 1. // Decay 12 lambdal = 0.01*p/86400;constant corresponding to leakage rate in seconds (1 day = 86400 seconds)13 // Using the data from Example 11.5 for the half life of Iodine -131 // Half $14 T_{12} = 8.04;$
```
life of Iodine 131 in days
15 lambdac = 0.693/(T_{12}*86400);
                                                  // Decay
       constant of Iodine -131 (I-131) in seconds
16 // Using data from Table 11.3
17 Eg_bar = 0.371;
                                                  11
      Average gamma decay energy per disintegration of
      I - 131 in MeV
18 // Using the plot given in Figure 11.11 and 11.12
      for Type F condition at 100 m
  sigma_y = 21;
                                                  //
19
      Horizontal dispersion coefficient
                                                  //
20 \text{ sigma_z} = 70;
      Vertical dispersion coefficient
21 // As lambdac*t \ll 1,
22 // Calculation
23 H = (0.262*Eg_bar*lambdal*C0*t0)/(%pi*v_bar*sigma_y*
      sigma_z);
24 // Result
25 printf(" \n The total external dose due to gamma ray
       exposure = \%.2E remn, H)
26
27 / / 2.
28 // Using the data given in Example 11.5
29 B = 2.32 \times 10^{(-4)};
                                                  //
      Normal breathing rate in m^3/sec
30 \text{ zeta} = 0.23;
                                                  //
      Fraction of core inventory in MeV
31 q = 0.23;
      Fraction of Iodine-131 in thyroid
32 M = 20;
                                                  // Mass
      of an adult thyroid in grams
33 // Calculation
34 H_dot = (592*B*zeta*q*lambdal*C0*t0)/(%pi*v_bar*
      sigma_v*sigma_z*M);
35 // Converting the units from rem/sec to milli-rem/
      hour by multiplying by (1000*3600)
36 // Result
37 printf(" \n The dose rate to an adult thyroid after
```

```
2 hours = \%.2E rem/sec or \%d mrem/hour\n", H_dot,
      ceil(H_dot*(1000*3600)));
38
39 // 3.
40 // Using the data given in Example 11.5
41 T_{12} = 8.04;
                                                    // Half
      life of Iodine 131 in days
42 T_{12b} = 138;
                                                    //
      Biological half life of Iodine 131 in days
  lambda = 0.693/(T_{12}*86400);
                                                    // Decay
43
       constant of Iodine -131 in sec<sup>(-1)</sup>
44 lambda_b = 0.693/(T_{12b}*86400);
                                                    11
      Biological decay constant of Iodine-131 in sec
      (-1)
45 // Calculation
46 H = H_dot/(lambda+lambda_b);
47 // Result
48 printf(" \n The dose commitment to thyroid by Iodine
      -131 exposure after 2 hours = \%.2 f rem \langle n, H \rangle;
```

Scilab code Exa 11.8 Direct dose from gamma rays

```
1 // Example 11.8
2 clear all;
3 \, \text{clc};
4
5 // Given
6 = 2.4;
                                                  //
     Energy of gamma rays in MeV
7 r = 1000 * 100;
     Distance from the building where radiation is
     exposed in cm
8 t0 = 2*3600;
                                                   // Time
     of exposure in seconds
9 A = 3*10^7;
                                                  //
```

Amount of initial radioactivity release due to Kr -88 in curie 10 f = 0.4; Fraction of disintegrations which release 2.4 MeV gamma rays 11 CO = A * f; 11 Effective number of curies $12 T_{12} = 2.79;$ // Half life of Iodine 131 in hours 1314 lambda = $0.693/(T_{12}*3600);$ // Decay constant of Iodine -131 in sec⁽⁻¹⁾ 15 // Using the result given in Example 11.7 $16 \text{ lambdal} = 1.16*10^{(-8)};$ // Decay constant corresponding to fission prouduct release from building 17 lambdac = lambda+lambdal; // Total decay constant in $\sec^{(-1)}$ // Using the data from Table II.4 for air at E = 2.418MeV $19 \text{ mu_rho} = 0.041;$ // The attenuation coefficient in cm^2/g 20 // Using standard value for density of air in g/cm³ 21 rho = $1.293 \times 10^{(-3)}$; $22 \text{ mu} = \text{mu}_{\text{rho}*\text{rho}};$ 23 // Using the data from Table II.5 for air at E = 2.4MeV // The $24 \text{ mua_rho} = 0.0227;$ ratio of absorption coefficient to density of air in cm^2/g 25 printf(" \n Buildup factor is measured at %.2f",mu*r); 26 // Using Berger's form in Problem 11.9 11 $27 B_p = 4.7;$ Buildup factor due to a point source 28 // Calculation 29 H = $(54*C0*(1-exp(-lambdac*t0))/lambdac)*(E*mua_rho*)$ $B_p * exp(-mu * r)/r^2);$

```
30 // Result
31 printf(" \n The direct dose due to gamma ray
exposure = %.4 f rem \n",H)
32 // There is a slight deviation in the answer due to
approximation of value in the textbook.
```

Scilab code Exa 11.9 Activity of radionuclide release into atmosphere

```
1 // Example 11.9
2 clear all;
3 \, \text{clc};
4
5 // Given data
6 \text{ gammai} = 0.0277;
                                                  //
      Fission yield of Iodine -131 in fraction
7 P = 3200;
                                                  //
      Thermal power of the plant in MW
8 // Calculation
9 alphai = 8.46*10^5*P*gammai;
10 // Result
11 printf(" \  \   The saturation activity of Iodine -131
      during reactor operation = \%.2E curie n, alphai)
12
13 // Using assumption 2 of Nuclear Regulatory
      Commission (NRC) in calculation of radii of
      exclusion zone and Low Population Zone (LPZ)
14 // Due to core meltdown, 25 percent of iodine
      inventory is released and out of which 91 percent
      is in elemental form.
15 Fp = 0.25 * 0.91;
      Fraction of Iodine -131 released from the fuel
      into the reactor containment
16 // As entire iodine escapes through air
17 \text{ Fb} = 1;
      Fraction of 'Fp' which remains airborne and is
```

```
capable of escaping from the building
18 // Calculation
19 CO = alphai*Fp*Fb;
20 // Result
21 printf(" \n The activity of Iodine-131 in elemental
form due to core meltdown = %.2E curie \n",CO);
```

Scilab code Exa 11.10 Concentration of radionuclide

```
1 // Example 11.10
2 clear all;
3 \text{ clc};
4
5 // Given data
6 P = 1000;
                                                          //
      Electrical power of the plant in Mwe
7 \text{ eta} = 0.38;
                                                          //
      Plant efficiency
8 P_{th} = P/eta;
                                                          //
      Thermal power of the plant in MW
9 h = 100;
                                                          //
      Height of stack in metre
10 t = 24*365;
                                                          //
      The number of hours in a year
11 \text{ m0} = 13000;
                                                          //
      Amount of coal in the plant in Btu/lb
12 \text{ mO}_ash = 0.09;
                                                          //
      Fraction of ash in the coal
13
14 // 1.
15 E = P_{th*t};
                                                          //
      Energy released in a year in MW-hour
16 // Converting the units in Btu by using 1 MW-hour =
      3.412*10^6 Btu
17 \text{ m} = (E*3.412*10^{6})/m0;
```

```
18 // Converting the units in g/year by using 1 lb/year
      = 453.59237 g/year
19 m = m * 453.59237;
20 // Assuming the fly ash equipment has an efficiency
      of 97.5% of fly ash removal
21 \text{ eta_flyash} = 0.025;
                                                        11
      Only (1-efficiency) is exhausted
22 m_ash = eta_flyash*m0_ash*m;
23 // A typical power plant contains 3pCi/g of each
      nuclide (Radium-226) in one year
24 \quad A = 3*10^{(-12)};
25 // Calculation
26 A_total = A*m_ash;
27 // Result
28 printf(" \n Total activity of Radium-226 emitted = \%
      .4 f curie \n",A_total)
29
30 / / 2.
31 v_bar = 1;
                                                        //
      Wind speed in m/sec
32 t = 24*365*3600;
                                                        11
      Analysis time of one year equivalently in seconds
33 \text{ MPC} = 3 \times 10^{(-12)};
                                                        11
      Maximum Permissible Concentration in micro-curie/
      cm^{3}
34 Q_bar = A_total/t;
                                                        11
      Emission rate for one year in curie/year
35 // Let the quantity chi*v_bar/Q_bar = x
36 // Using the plot for Pasquill F, given in Fig. A.7,
      Pg no 413 from Slade, D. H., Editor, Meteorology
       and Atomic Energy -1968. U. S. Atomic Energy
      Commission Report TID-24190, 1968.
37 x = 2.5 \times 10^{(-6)};
                                                        //
     Maximum value of x at 10<sup>4</sup> m
38 // Solving for chi
39 chi = (x*Q_bar)/v_bar;
40 // Converting the units from Ci/m<sup>3</sup> to micro-curie/
      cm<sup>3</sup> by multiplying by 10^{6}/10^{6} = 1
```

```
41 printf(" \n Concentration of Radium-226 present = %
    .2E micro-curie/cm^3 \n",chi)
42 // Let c be the comparison factor
43 // Calculation
44 c = MPC/chi;
45 // Result
46 printf(" \n On comparison, the total concentration
    of Radium-226 is %d times smaller than Maximum
    Permissible Concentration (MPC) \n",c)
47 // The comparison factor is slightly different from
    the value in the textbook. This is because of
    approximation used in the textbook.
```

Scilab code Exa 11.11 Activity of radioactive gas effluent

```
1 // Example 11.11
2 clear all;
3 \text{ clc};
4
5 // Given data
6 Qy_bar = 1.04*10^{(-2)};
                                                    //
      Emission rate for one year in curie/year
7 // Let (chi/Q_bar) = d which is called 'Dilution
      factor'
8 d = 4*10^{(-8)};
                                                    //
      Dilution factor in year/cm<sup>3</sup>
9 \text{ vd} = 0.01;
                                                    //
      Experimentally determined constant
10
11 // 1.
12 T_{12} = 8.04;
                                                    // Half
      life of Iodine 131 in days
13 T_12f = 14;
                                                    // First
       order half life of Iodine 131 in days
14 // Converting days into years by using 1 year = 365
```

```
davs
15 lambda = 0.693/(T_{12}/365);
                                                        // Decay
        constant of Iodine - 131
                                                        // First
16 lambdaf = 0.693/(T_12f/365);
        order decay constant of Iodine - 131
17 // Calculation
18 Cf = (Qy_bar*d*vd)/(lambda+lambdaf);
19 // Expressing the result in micro-curie
20 \text{ Cf} = \text{Cf} * 10^{6};
21 // Result
22 printf(" \n The activity of I-131 on the vegetation
      = \%.2E micro-curie/m<sup>2</sup> \n", Cf);
23
24 // 2.
25 // The proportionality factor has a value 9*10^{(-5)}
      Ci/cm<sup>3</sup> of milk per Ci/m<sup>2</sup> of grass
26 // Calculation
27 Cm = 9*10^{(-5)}*Cf;
28 // Result
29 printf(" \n The concentration of I-131 in the milk =
       \%.2E micro-curie/m<sup>2</sup> \n", Cm);
30
31 // 3.
32 \text{ MPC} = 3 \times 10^{(-7)};
      Maximum Permissible Concentration in micro-curie/
      cm^{3}
33 // Calculation
34 \text{ H_dot} = (2270 * \text{Cm}) / \text{MPC};
35 // Result
36 printf(" \n The annual dose rate to an infant
       thyroid by consuming radiated milk = \%.2E mrem/
      year \langle n^{"}, H_{dot} \rangle;
```

Scilab code Exa 11.12 Activity of radioactive liquid effluent

```
1 // Example 11.12
2 clear all;
3 \text{ clc};
4
5 // Given data
6 \, Qy_{bar} = 0.197;
      Emission rate for one year in micro-curie/year
7 // Let (chi/Q_bar) = d which is called 'Dilution
      factor'
8 d = 6.29 * 10^{(-16)};
                                                    //
      Dilution factor in year/cm<sup>3</sup>
9 MPC_w = 6*10^{(-5)};
                                                    11
      Maximum Permissible Concentration (MPC) of iron
      in micro-curie/cm^3
10
                                                    // The
11 Cw = Qy_bar*d;
      concentration of Fe-59
12 // For fish
13 \text{ Rs_fish} = 110;
                                                   11
      Consumption rate in g/day
14 // Using the data from Table 11.15 for saltwater
      concentration of fish for iron
15 \text{ CF}_{fish} = 1800;
                                                   //
      Concentration Factor of fish
16 Cs_fish = CF_fish*Cw;
                                                    //
      Activity of fish
17 H_dot_fish = (Cs_fish*Rs_fish*500)/(MPC_w*2200);
      // Dose rate for fish
18
19 // For mollusks
                                                   11
20 Rs_mollusk = 10;
      Consumption rate in g/day
21 // Using the data from Table 11.15 for saltwater
      concentration of mollusk for iron
22 \text{ CF}_{mollusk} = 7600;
                                                   //
      Concentration Factor of mollusk
23 Cs_mollusk = CF_mollusk*Cw;
                                                    //
      Activity of mollusk
```

```
24 H_dot_mollusk = (Cs_mollusk*Rs_mollusk*500)/(MPC_w
               // Dose rate for mollusk
      *2200);
25
26 // For crustaceans
27 Rs_crustacean = 10;
                                               11
     Consumption rate in g/day
  // Using the data from Table 11.15 for saltwater
28
     concentration of crustacean for iron
29 CF crustacean = 2000:
                                               //
     Concentration Factor of crustacean
30 Cs_crustacean = CF_crustacean*Cw;
                                                //
      Activity of crustacean
31 H_dot_crustacean = (Cs_crustacean*Rs_crustacean*500)
     /(MPC_w*2200); // Dose rate for crustacean
32
33 // Calculation
34 H_dot = H_dot_fish+H_dot_mollusk+H_dot_crustacean;
35 // Result
36 printf(" \n The annual dose rate to GI tract by
     consuming fish = %.2E mrem/year", H_dot_fish);
37 printf(" \n The annual dose rate to GI tract by
     consuming mollusk = \%.2E mrem/year", H_dot_mollusk
     );
38 printf(" \n The annual dose rate to GI tract by
     consuming crustaceans = \%.2E mrem/year",
     H_dot_crustacean);
39 printf(" \n The annual dose rate to GI tract by
     consuming seafood = \%.2E mrem/year \n", H_dot);
40 // The answer for annual dose rate to GI tract by
     consuming fish is wrong in the textbook. This is
     because the value of fish consumption rate is
     wrongly considered.
```